



**1095 Kingston Road Ltd. C/O Resident**

# **Noise Assessment**

**1095 Kingston Road, Pickering, Ontario**

**February 2025 – 24-9327**

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- B D-6 Classification Criteria
- C Traffic Data
- D Stamson Outputs
- E BPN Analysis

### References

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## Acronyms, Abbreviations, Definitions

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AADT	Average Annual Daily Traffic
BPN56	Building Practice Note 56
dBa	Decibels, A-weighted
CN	Canadian National Railway
Dillon	Dillon Consulting Limited
FHWA	Federal Highway Administration
FTA/FRA	Federal Transit Administration/Federal Railroad Administration
HVAC	Heating, ventilation, and air conditioning
Hz	Hertz
ISO	International Organization for Standardization
kg/m <sup>2</sup>	kilograms per square metre
km	kilometre
km/hr	kilometres per hour
L <sub>eq</sub>	Equivalent continuous sound level
m	metre
MECP	Ministry of Environment, Conservation and Parks
mm/s	millimetres per second
MTO	Ministry of Transportation Ontario
NRC	National Research Council's
OLAs	Outdoor Living Areas
OS	Open Space

POR	Points of reception
RMS	Root Mean Square
SPA	Site Plan Approval
STC	Sound Transmission Class
TNM	Transportation Noise Model

## 1.0

# Introduction

## 1.1

## Purpose and Objective

Dillon Consulting Limited (Dillon) was retained by 1095 Kingston Road Ltd. C/O Resident to complete a noise and vibration assessment as requested by the Region of Durham for the 1095 Kingston Road proposed development. The proposed development consists of four residential towers, located west of Dixie Road, south of Kingston Road, and north of Highway 401 in Pickering, Ontario. This study has been completed in support of the submission application for the proposed development.

The noise and vibration assessment presented herein was prepared in accordance with the guidelines and requirements of the Region of Durham and the Ontario Ministry of Environment, Conservation and Parks (MECP) noise publication NPC-300. The assessment focuses on noise impacts from the surrounding environment on the proposed development.

The purpose of the noise assessment is to ultimately create a suitable acoustical environment for the protection of residents of the proposed noise sensitive land uses, to protect existing and/or formally approved transportation corridors, and to create compatible land uses and avoid potential adverse effects due to noise.

## 1.2

## The Project and Surrounding Areas

The proposed development is located to the west of Dixie Road, south of Kingston Road, and north of the Highway 401 in Pickering, Ontario. There are commercial businesses and railway lines in the immediate vicinity of the proposed development parcel. Located to the north and west are residential properties, located to the east are commercial businesses, and located to the south are railway lines and the Highway 401. The subject site and surrounding area are shown in **Figure 1**.

Currently, the proposed development land parcel is a commercial plaza. The proposed development consists of four towers that are each 35 storeys.

The land of the proposed development is currently subject to the Kingston Road Corridor and Special Retailing Node Intensification Area and are not subject to the

zoning by-law 3036. Immediately surrounding the proposed development are the following zoned lands:

- North – Residential (S2-DB per by-law 6992/09) and Commercial General (C1 per by-law 6535/05);
- East – Kingston Road Corridor and Special Retailing Node Intensification Area;
- South – Open Space (OS); and
- West – Residential (S2-DB per by-law 6992/09).

The concept plan of the proposed development and zoning map is provided in **Appendix A**.

## 2.0 Impacts from the Environment on the Proposed Development

A review of the site and surrounding area has been conducted to determine potential stationary noise sources associated with commercial and industrial properties in proximity of the proposed development as well as potential noise impacts from transportation sources (road and rail).

### 2.1 Stationary Noise

The MECP's land-use compatibility guidelines (D-series) are intended to prevent or minimize the encroachment of sensitive land uses upon industrial/commercial land uses and vice versa, as these two types of land uses are normally incompatible, due to possible adverse effects on the sensitive land use. The guidelines were designed to reduce potential complaints and protect sensitive land uses while upholding the ability of commercial and industrial properties to maintain compliance with MECP requirements.

The D-6 guideline separates industries into three classes based on the scale of the industry's operation. This involves considerations including, but not limited to: probability of fugitive emissions, schedule of operations, and production volume. The D-6 criteria for industry classification are shown in **Appendix B**. The guideline provides setback distances for each class representing potential influence areas and recommended minimum separation distances shown in **Table 1**.

**Table 1: D-6 Influence Areas and Recommended Separation Distances**

Industrial Class	Potential Influence Area	Recommended Minimum Separation Distance
Class I	70 metres (m)	20 m
Class II	300 m	70 m
Class III	1000 m	300 m

The D-6 guideline specifies that for site-specific plans, measurement shall be from the closest existing, committed, or proposed property/lot line of the industrial land use to the property/lot line of the closest existing, committed, or proposed sensitive land use.

Areas designated for ancillary land uses that are not of a sensitive nature (such as a parking lot) may be included within the separation distance.

When considering vacant industrial land, determination of its potential influence area is based on a hypothetical “worst case scenario” for which the zoned area is committed.

## 2.2 Nearby Industries

Dillon reviewed the area surrounding the subject lands in order to classify the existing industrial and commercial lands using the MECP’s D-Series framework, as well as to identify nearby vacant lands which are zoned to allow for commercial or industrial uses. Additionally, a site visit was conducted by Dillon personnel on December 3rd, 2024, to identify industrial or commercial operations with the potential influence areas that intersect the proposed development.

Industries were classified based on site visit observations, review of existing MECP approvals documents, and through publicly available information.

Within the study area, the only industry identified with potential for adverse effects on the proposed development was the commercial plaza located at 1099 Kingston Road and approximately 30 m east of the proposed development’s property boundary. Based on observations made during the site visit, the commercial plaza is considered a Class I industry with the potential to have noise impacts on the proposed development.

As per the D-6 Guideline, the proposed development is located within the potential influence area of the commercial plaza. The following sections provide an assessment of the potential noise impacts from the commercial plaza on the proposed development.

### 2.2.1 Noise Sources

The only potential noise source Dillon identified associated with the commercial plaza were rooftop heating, ventilation, and air conditioning (HVAC) units. Dillon assessed 22 rooftop HVAC units. Conservatively, it was assumed that the rooftop HVAC units operate simultaneously during the daytime and evening period. HVAC units were assumed to run at 50% duty cycle during the nighttime period.

Dillon utilized its in-house library to apply sound power levels to the identified noise sources.

## 2.2.2

**Noise Criteria**

NPC-300 defines sound level limits for noise impacts from stationary sources on noise sensitive land uses. A noise sensitive land use is defined as a property of a person that accommodates a dwelling, a noise sensitive commercial purpose, or a noise sensitive institutional purpose. This definition includes:

- Permanent, seasonal, and rental residences;
- Hotels, motels, and campgrounds;
- Schools, universities, libraries, and daycare centres;
- Hospitals and clinics, nursing/retirement homes; and
- Places of worship.

Points of reception (POR) for dwellings are located at the centre of any window on a noise sensitive space, with a first-storey height of 1.5 metre (m) and subsequent storeys separated by 3 m. A dwelling may have an outdoor point of reception located on its property within 30 m of its façade at a height of 1.5 m, typically in back or front yards, terraces, or patios.

In NPC-300, areas are divided into four classes based on their existing background acoustical environment:

- Class 1 – Urban Area;
- Class 2 – Semi-Urban/Semi-Rural Area;
- Class 3 – Rural Area; and
- Class 4 – Areas of Redevelopment and Infill.

The sound level limits for outdoor and plane-of-window PORs for continuous noise, in decibels A-weighted (dBA), are outlined in **Table 2**.

**Table 2 Notes**

[1] The plane of window for living area or sleeping quarters will be referred to as the “façade” of a receptor.

**Table 2: Stationary Source Continuous Noise Exclusionary Limits**

Assessment Location	Time of Day	Class 1 Area	Class 2 Area	Class 3 Area	Class 4 Area
Plane of window for living area or sleeping quarters <sup>[1]</sup>	Daytime (07:00 to 19:00)	50 dBA	50 dBA	45 dBA	60 dBA
	Evening (19:00 to 23:00)	50 dBA	50 dBA	40 dBA	60 dBA
	Nighttime (23:00 to 07:00)	45 dBA	45 dBA	40 dBA	55 dBA
Outdoor points of reception	Daytime (07:00 to 19:00)	50 dBA	50 dBA	45 dBA	55 dBA
	Evening (19:00 to 23:00)	50 dBA	45 dBA	40 dBA	55 dBA

Based on observations made during the site visit completed on October 9, 2024, the existing background acoustical environment of the proposed development's lands are considered Class 1 – Urban Area.

## 2.2.2.1

**Background Sound Levels**

In areas that have increased ambient noise due to road traffic, the background sound level may be used as the stationary sound level limit. Due to the proposed development's proximity to Highway 401, transportation noise analysis was completed to determine the background sound levels for the receptors of the proposed development.

The background sound levels due to road noise was determined based on the minimum hourly noise impacts during the daytime, evening, and nighttime periods. Dillon utilized hourly traffic counts over a one-week measurement period for Highway 401 to determine the minimum hourly road noise impacts on the proposed development. Truck percentages for Highway 401 were provided by the Ministry of Transportation Ontario (MTO). Traffic data utilized in this assessment has been provided in **Appendix C**.

The road noise analysis was completed using the STAMSON ORNAMENT protocol. **Table 3** below summarizes the calculated background sound levels for the point of reception of the proposed development with the greatest proximity and exposure to the commercial plaza.



**Table 3: Background Sound Levels**

Receptor	Time Period	Background Sound Level (1 hour) (dBA)
Tower 2B 8th Storey Podium East Façade	Daytime (07:00 to 19:00)	63
	Evening (19:00 to 23:00)	65
	Nighttime (23:00 to 07:00)	60

The output files used to calculate the background sound levels have been included in **Appendix D**.

### 2.2.3 Predicted Sound Levels

The stationary noise analysis was completed using CADNA/A, an outdoor noise propagation model, based on International Organization for Standardization (ISO) Standard 9613, Part 1: Calculation of the absorption of sound by the atmosphere, 1993 and Part 2: General method of calculation (ISO-9613-2:1996). The model is capable of incorporating various site-specific features, such as elevation, berms, absorptive grounds, and barriers to accurately predict noise levels at specific receptors, pertaining to noise emissions from a particular source / sources. The ISO based model accounts for reduction in sound level due to increased distance and geometrical spreading, air absorption, ground attenuation, and acoustical shielding by intervening structures and topography. The model is considered conservative as it represents atmospheric conditions that promote propagation of sound from the source to the receiver.

The following assumptions were incorporated in the noise propagation modelling:

- A global ground absorption coefficient of 0.50, representing a mix of reflective and absorptive grounds of the area surrounding the proposed development.
- Second order reflection was incorporated in the noise model; and
- The ground within the study area is considered to be generally flat.

Impacts from the stationary noise sources were predicted through noise propagation modelling. **Table 4** below summarizes the worst-case noise impacts on the façades of the proposed development for continuous noise.

**Table 4: Noise Impact Summary Table**

Point of Reception	Time Period	Maximum Leq (1 hour) (dBA)	MECP Compliance
Tower 2B 6 <sup>th</sup> Storey Podium East Façade	Daytime (07:00 to 19:00)	54	Compliant with background noise level criteria
	Evening (19:00 to 23:00)	54	Compliant with background noise level criteria
	Nighttime (23:00 to 07:00)	51	Compliant with background noise level criteria

The predicted noise impacts from the commercial plaza on the proposed development have been shown in **Figure 2**. Stationary noise impacts at the remaining points of receptions of the proposed development have been compared against the applicable noise criteria.

The results indicate that the potential noise impacts from the commercial plaza on the proposed development are predicted to be compliance with the MECP's NPC-300.

### 2.3 Transportation Noise Assessment

The transportation sources identified with the potential to impact the proposed development include vehicular traffic along Kingston Road and the Highway 401 and rail traffic along the Canadian National Railway (CN) York Subdivision, CN Kingston Subdivision, and Metrolinx railways. Impacts from road and rail traffic were predicted and compared against the applicable criteria in the MECP noise guideline publication, **NPC 300 – Environmental Noise Guideline – Stationary and Transportation Sources – Approvals and Planning (2013)**. NPC-300 outlines noise level criteria for sensitive land uses, which assist in determining requirements for façade construction, ventilation requirements, warning clauses, and potential noise barriers for the proposed development.

## 2.3.1

## Noise Criteria

The applicable transportation noise criteria, as outlined in Part C of NPC-300, is summarized below, and presented in **Table 5** through to **Table 9**.

**Table 5** summarizes the indoor sound level limits based on the type of space assessed, time of day, and the maximum allowable equivalent sound levels from roadways and railways. The indoor noise levels are based on the assumption of closed windows and doors.

**Table 5: Indoor Sound/Level Limits for Road and Rail**

Type of Space	Time Period	Equivalent Sound Level - $L_{eq}$ Road	Equivalent Sound Level - $L_{eq}$ Rail
Living/dining areas of residences, hospitals, nursing homes, schools, daycares, etc.	Daytime 07:00 to 23:00	45 dBA	40 dBA
Living/dining areas of residences, hospitals, nursing homes, etc. (except schools and daycares)	Nighttime 23:00 to 07:00	45 dBA	40 dBA
Sleeping quarters of residences	Daytime 07:00 to 23:00	45 dBA	40 dBA
	Nighttime 23:00 to 07:00	40 dBA	35 dBA

**Table 6** outlines the maximum equivalent sound levels, from roadway and railway sources, where if exceeded a detailed building component design assessment is required to ensure the indoor sound level limits (see **Table 5**) are achieved.

**Table 6: Requirements for Building Component Assessment**

Assessment Location	Time Period	Equivalent Sound Level - $L_{eq}$ Road	Equivalent Sound Level - $L_{eq}$ Rail
Plane of window for living area or sleeping quarters	Daytime 07:00 to 23:00	65 dBA	60 dBA
	Nighttime 23:00 to 07:00	60 dBA	55 dBA

As per MECP's NPC-300 Noise Guideline, **Table 7** outlines the façade construction requirements for proposed residential developments within 100 m of rail tracks.

**Table 7: Façade Construction Requirement**

Assessment Location	Equivalent Sound Level - $L_{eq}$ 24 hour	Façade Construction Requirements
Plane of window for living area or sleeping quarters	> 60 dBA	Brick veneer or acoustical equivalent
	≤ 60 dBA	No requirement

**Table 8** summarizes potential noise warning clauses and ventilation requirements that should be used to warn of potential annoyance due to existing noise sources related to transportation.

**Table 8: Ventilation and Warning Clause Requirement**

Assessment Location	Time Period	Equivalent Sound Level - $L_{eq}$ Road and Rail	Ventilation and Warning Clause Requirements
Plane of window for living area or sleeping quarters	Daytime (07:00 to 23:00)	≤ 55 dBA	No requirement
		> 55 dBA and ≤ 65 dBA	Provision for the installation of central air conditioning with a Type C warning clause
		> 65 dBA	Installation of central air conditioning with a Type D warning clause

Assessment Location	Time Period	Equivalent Sound Level - $L_{eq}$ Road and Rail	Ventilation and Warning Clause Requirements
Plane of window for living area or sleeping quarters	Nighttime (23:00 to 07:00)	$\leq 50$ dBA	No requirement
		$> 50$ dBA and $\leq 60$ dBA	Provision for the installation of central air conditioning with a Type C warning clause
		$> 60$ dBA	Installation of central air conditioning with a Type D warning clause

The applicable noise criteria for Outdoor Living Areas (OLAs) specific to surface transportation are presented in **Table 9**. If the 16-Hour Equivalent Sound Level -  $L_{eq}$  16 hour (16h) at an OLA is greater than 55 dBA and less than or equal to 60 dBA, noise control measures may be applied to reduce the sound level to 55 dBA. Otherwise, prospective purchasers or tenants should be informed of potential elevated noise levels by way of warning clause Type A. For a  $L_{eq}$  16h of greater than 60 dBA, noise mitigation measures are required to reduce the noise levels to 55 dBA or less.

**Table 9: OLA Level Limits for Road and Rail**

Assessment Location	Equivalent Sound Level - $L_{eq}$ 16h Road and Rail	Noise Control Measures and Warning Clause Requirements
Outdoor Living Areas	$\leq 55$ dBA	No requirement
	$> 55$ dBA and $\leq 60$ dBA	Installation of noise control measures <b>OR</b> a Type A warning clause
	$> 60$ dBA	Installation of noise control measures to reduce noise level to $< 55$ dBA <b>OR</b> Installation of noise control measures to reduce noise level to $> 55$ dBA and $\leq 60$ dBA with a Type B warning clause

## 2.3.2 Transportation Sources

In assessing potential transportation noise impacts on the proposed development, the following transportation corridors were considered:

- Kingston Road;
- Highway 401;
- CN York Subdivision;
- CN Kingston Subdivision; and
- GO Transit Lakeshore East Subdivision.

## 2.3.2.1 Road Noise Sources

Road traffic information for Kingston Road was provided by the Regional Municipality of Durham. The provided data included the future forecasted Average Annual Daily Traffic (AADT), the percent of trucks, ratio of heavy to medium trucks, and posted speed. It was assumed that 90% of traffic occurs during the daytime period, and 10% during the nighttime period.

Road traffic information for Highway 401 was provided by the MTO. The provided data included the AADT for the year 2021, the percentage of trucks, and hourly traffic counts for Highway 401 Eastbound Express, Westbound Collector, and Westbound Express. An annual growth rate of 1.8% was determined for this section of the Highway 401 based on 10 years of historical AADTs. Based on the hourly traffic counts, it was determined that 83% of traffic on the Highway 401 occurs during the daytime period and 17% during the nighttime period. Based on the MTO guide for completing noise assessments, it was assumed that 75% of truck traffic is heavy trucks and 25% is medium trucks. Highway 401 traffic volumes were forecasted to the year 2035.

The forecasted future road traffic data is presented in **Table 10**.

**Table 10: Future Road Traffic Data**

Roadway	Forecasted AADT	Medium Trucks	Heavy Trucks	Speed (kilometers per hour [km/hr])
Kingston Road	35,000	5.6%	2.4%	60
Highway 401	344,684	2.5%	7.5%	100

## 2.3.2.2 Rail Noise Sources

Dillon requested rail traffic information from Canadian National Railway (CN) for the Kingston Subdivision and York Subdivision. At the time of this assessment, CN has not provided information specific to rail operations in proximity to 1095 Kingston Road. Dillon used historic rail traffic information for the CN Kingston and York Subdivision from a previous project in close proximity to the proposed development.

Rail traffic information for CN Kingston Subdivision was developed using information provided by CN in proximity to 705 Kingston Road. The provided rail traffic information included the number of freights, way freights, and passenger trains travelling on the CN Kingston Subdivision during the daytime and nighttime periods. Additionally, the maximum number of locomotives and cars, and the maximum speed was provided for each train type. CN recommended that a 2.5% annual growth rate be used for forecasting future rail traffic volumes. CN Kingston Subdivision traffic volumes were forecasted to the year 2035.

The volume of trains and train speed for the CN York Subdivision was developed using the Government of Canada's Grade Crossing Inventory. The information provided by CN for the CN Kingston Subdivision was used to determine the locomotives and cars per train, as well as the annual growth rate. It was conservatively assumed that all trains operating on the CN York Subdivision are freights and are equally distributed throughout the daytime and nighttime. CN York Subdivision traffic volumes were forecasted to the year 2035.

Rail traffic information for GO Transit was provided by Metrolinx. They provided rail traffic information including the forecasted diesel and electric GO train volumes, the number of locomotives and cars, and the maximum speed. Metrolinx identified that the use of diesel trains in acoustic modelling is preferred.

The forecasted future rail traffic data is presented in **Table 11** and **Table 12**.

**Table 11: Future Rail Traffic Data - Daytime and Evening (07:00 to 23:00)**

Rail Operator	Train Type	Locomotives	Cars	Speed (km/h)
CN York Subdivision	Freight	106	3704	80

Rail Operator	Train Type	Locomotives	Cars	Speed (km/h)
CN Kingston Subdivision	Freight	63	2204	105
	Way Freight	0	0	105
	Passenger	89	446	161
GO Transit	Passenger	277	1385	161

**Table 12: Future Rail Traffic Data – Nighttime (23:00 to 07:00)**

Rail Operator	Train Type	Locomotives	Cars	Speed (km/h)
CN York Subdivision	Freight	53	1852	80
CN Kingston Subdivision	Freight	26	918	105
	Way Freight	21	131	105
	Passenger	3	13	161
GO Transit	Passenger	47	385	161

Based on information received from Metrolinx, anti-whistling bylaws are not in effect for the at-grade crossings in proximity to the proposed development. However, no at-grade crossings were identified within 1 kilometre (km) of the proposed development. Therefore, with the exception of emergency events, train whistle noise is not expected in proximity to the proposed development and was therefore not considered in this assessment.

### 2.3.3 Predicted Sound Level

The noise analysis was completed using Cadna/A, a noise propagation software. The Cadna/A software includes the implementation of the Transportation Noise Model (TNM) roadway algorithms, as well as the Federal Transit Administration/Federal Railroad Administration (FTA/FRA) railway algorithms. The model is capable of incorporating various site specific features, such as elevation, berms, absorptive grounds, and barriers to accurately predict noise levels at specific receptors, pertaining to noise emissions from a particular noise source. The model accounts for reduction in sound level due to increased distance and geometrical spreading, air absorption, ground attenuation, and acoustical shielding by intervening structures and topography. The model is considered conservative as it represents atmospheric conditions that promote propagation of sound from source to receptor.



### Railway Analysis

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The railway noise impact assessment was conducted using the FRA algorithm using Cadna/A. The STEAM, utilized through STAMSON Version 5.04 was not used in the assessment due to the complexity of the proposed development and the surrounding area. Based on Dillon's experience using FRA and STEAM in rail noise assessments, the results of the FRA algorithm are within an acceptable range of accuracy.

### Roadway Analysis

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The assessment for roadway impact noise was completed using the TNM algorithm, developed by the Federal Highway Administration (FHWA), implemented through Cadna/A. The ORNAMENT, utilized through STAMSON Version 5.04 was not used in the assessment due to the complexity of the proposed development and the surrounding area. STAMSON is not capable of incorporating the 3-dimensional components of the proposed development and accurately predicting transportation noise impacts for elevated receptors. Based on Dillon's experience using TNM and ORNAMENT in road noise assessments, the results of the ORNAMENT algorithm are within an acceptable range of accuracy.

Comparative modelling using STAMSON was performed to confirm the accuracy of the TNM protocol. The comparative modelling has been presented in **Section 2.4**.

#### 2.3.3.1

### Sensitive Receptor Locations

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The site plan of the proposed development was reviewed to identify the location of sensitive receptors. Representative noise receptors were selected for each façade of the buildings of the proposed development and were assessed for transportation noise impacts.

In addition to façade locations, transportation noise impacts were assessed at Outdoor Living Area (OLA) locations. Per NPC-300, common OLAs were assessed at the outdoor amenity areas located on the 7<sup>th</sup> floor terrace of Tower 1 and the 5<sup>th</sup> floor terrace of Tower 2.

Additional outdoor amenity areas are located throughout the proposed development, however, it is not expected that the predicted noise impacts on the remaining outdoor amenity areas can be feasibly mitigated with acoustic barriers. The OLAs located on the

7<sup>th</sup> floor terrace of Tower 1 and the 5<sup>th</sup> floor terrace of Tower 2 are intended and designed for the quiet enjoyment of the outdoor environment for the occupants of the proposed development.

The locations of the noise receptors assessed in this study has been shown in **Figure 3**.

## 2.3.3.2

**Transportation Noise Impacts – Plane of Window**

**Table 13** summarizes the predicted building façade noise levels from transportation noise sources at the representative sensitive receptors within the proposed development.

**Table 13 Notes**

[1] Predicted noise levels that exceed the applicable limits are presented in **bold**.

[2] Tower 2 is greater than 100 m from the nearest rail tracks and does not require facade construction assessment based on 24 hour rail impacts

**Table 13: Transportation Noise Prediction Summary Table - Façade Impacts**

<b>Receptor</b>	<b>Time Period</b>	<b>Equivalent Sound Level - <math>L_{eq}^{[1]}</math> [dBA] Road Impacts</b>	<b>Equivalent Sound Level - <math>L_{eq}^{[1]}</math> [dBA] Railway Impacts</b>	<b>Equivalent Sound Level - <math>L_{eq}^{[1]}</math> [dBA] Combined Road and Rail</b>	<b>Equivalent Sound Level - <math>L_{eq}^{[1]}</math> [dBA] 24 Hour Rail<sup>[2]</sup></b>
Tower 1 L2 to L6 North	Daytime	69	64	70	62
	Nighttime	64	63	67	62
Tower 1 L2 to L6 East	Daytime	75	69	76	64
	Nighttime	72	67	73	64
Tower 1 L2 to L6 South	Daytime	79	73	80	68
	Nighttime	75	71	76	68
Tower 1 L7 to L8 North	Daytime	68	65	70	62
	Nighttime	63	64	67	62
Tower 1 L7 to L8 East	Daytime	75	70	76	64
	Nighttime	72	68	73	64
Tower 1 L7 to L8 South	Daytime	80	73	80	70
	Nighttime	76	72	77	70
Tower 1 L7 to L8 West	Daytime	74	69	75	67
	Nighttime	69	68	72	67
Tower 1A L9 to L35 North	Daytime	70	65	71	59
	Nighttime	66	63	68	59

Receptor	Time Period	Equivalent Sound Level - $L_{eq}^{[1]}$ [dBA] Road Impacts	Equivalent Sound Level - $L_{eq}^{[1]}$ [dBA] Railway Impacts	Equivalent Sound Level - $L_{eq}^{[1]}$ [dBA] Combined Road and Rail	Equivalent Sound Level - $L_{eq}^{[1]}$ [dBA] 24 Hour Rail <sup>[2]</sup>
Tower 1A L9 to L35 East	Daytime	77	71	78	67
	Nighttime	73	70	75	67
Tower 1A L9 to L35 South	Daytime	79	73	80	70
	Nighttime	75	72	77	70
Tower 1A L9 to L35 West	Daytime	74	69	75	67
	Nighttime	69	68	72	67
Tower 1B L9 to L35 North	Daytime	69	65	70	62
	Nighttime	64	64	67	62
Tower 1B L9 to L35 East	Daytime	73	68	74	63
	Nighttime	69	66	71	63
Tower 1B L9 to L35 South	Daytime	76	71	77	66
	Nighttime	73	69	74	66
Tower 1B L9 to L35 West	Daytime	71	67	72	64
	Nighttime	67	66	69	64
Tower 2 L2 to L4 North	Daytime	73	67	74	NA
	Nighttime	69	65	71	NA
Tower 2 L2 to L4 East	Daytime	68	63	69	NA
	Nighttime	63	62	66	NA

<b>Receptor</b>	<b>Time Period</b>	<b>Equivalent Sound Level - <math>L_{eq}^{[1]}</math> [dBA] Road Impacts</b>	<b>Equivalent Sound Level - <math>L_{eq}^{[1]}</math> [dBA] Railway Impacts</b>	<b>Equivalent Sound Level - <math>L_{eq}^{[1]}</math> [dBA] Combined Road and Rail</b>	<b>Equivalent Sound Level - <math>L_{eq}^{[1]}</math> [dBA] 24 Hour Rail<sup>[2]</sup></b>
Tower 2 L2 to L4 South	Daytime	<b>76</b>	<b>70</b>	<b>77</b>	NA
	Nighttime	<b>73</b>	<b>68</b>	<b>74</b>	NA
Tower 2 L2 to L4 West	Daytime	<b>69</b>	<b>63</b>	<b>70</b>	NA
	Nighttime	<b>64</b>	<b>62</b>	<b>66</b>	NA
Tower 2 L5 to L6 North	Daytime	<b>68</b>	<b>66</b>	<b>70</b>	NA
	Nighttime	<b>64</b>	<b>64</b>	<b>67</b>	NA
Tower 2 L5 to L6 East	Daytime	<b>74</b>	<b>69</b>	<b>75</b>	NA
	Nighttime	<b>70</b>	<b>67</b>	<b>72</b>	NA
Tower 2 L5 to L6 South	Daytime	<b>77</b>	<b>71</b>	<b>78</b>	NA
	Nighttime	<b>73</b>	<b>69</b>	<b>75</b>	NA
Tower 2 L5 to L6 West	Daytime	<b>70</b>	<b>65</b>	<b>71</b>	NA
	Nighttime	<b>66</b>	<b>63</b>	<b>68</b>	NA
Tower 2A L7 to L35 North	Daytime	<b>69</b>	<b>65</b>	<b>70</b>	NA
	Nighttime	<b>65</b>	<b>63</b>	<b>67</b>	NA
Tower 2A L7 to L35 East	Daytime	<b>71</b>	<b>67</b>	<b>73</b>	NA
	Nighttime	<b>68</b>	<b>65</b>	<b>70</b>	NA
Tower 2A L7 to L35 South	Daytime	<b>70</b>	<b>67</b>	<b>72</b>	NA
	Nighttime	<b>66</b>	<b>65</b>	<b>69</b>	NA

**1095 Kingston Road Ltd. C/O Resident**

Noise Assessment - 1095 Kingston Road, Pickering, Ontario

February 2025 – 24-9327

Receptor	Time Period	Equivalent Sound Level - $L_{eq}^{[1]}$ [dBA] Road Impacts	Equivalent Sound Level - $L_{eq}^{[1]}$ [dBA] Railway Impacts	Equivalent Sound Level - $L_{eq}^{[1]}$ [dBA] Combined Road and Rail	Equivalent Sound Level - $L_{eq}^{[1]}$ [dBA] 24 Hour Rail <sup>[2]</sup>
Tower 2A L7 to L35 West	Daytime	<b>68</b>	<b>64</b>	<b>70</b>	NA
	Nighttime	<b>63</b>	<b>63</b>	<b>66</b>	NA
Tower 2B L7 to L35 North	Daytime	63	59	<b>64</b>	NA
	Nighttime	59	<b>57</b>	<b>61</b>	NA
Tower 2B L7 to L35 East	Daytime	<b>75</b>	<b>69</b>	<b>76</b>	NA
	Nighttime	<b>71</b>	<b>67</b>	<b>73</b>	NA
Tower 2B L7 to L35 South	Daytime	<b>79</b>	<b>72</b>	<b>80</b>	NA
	Nighttime	<b>75</b>	<b>70</b>	<b>76</b>	NA
Tower 2B L7 to L35 West	Daytime	<b>72</b>	<b>67</b>	<b>73</b>	NA
	Nighttime	<b>68</b>	<b>65</b>	<b>70</b>	NA

The predicted transportation sound levels at the proposed development are presented in **Figure 3**, for daytime impacts.

### 2.3.3.3 Transportation Noise Impacts – Outdoor Living Areas (OLA)

**Table 14** summarizes the worst-case predicted transportation noise levels at the OLAs of the proposed development.

#### Table 14 Notes

[1] Predicted noise levels that exceed the applicable limits are presented in **bold**.

**Table 14: Transportation Noise Prediction Summary Table - OLA Impacts**

Assessment Location	Daytime Equivalent Sound Level - $L_{eq}$ 16-hr <sup>[1]</sup> (dBA)
Tower 1 – 7 <sup>th</sup> Floor OLA	<b>61</b>
Tower 2 – 5 <sup>th</sup> Floor OLA	<b>67</b>

### 2.3.4 Noise Control Measures

#### 2.3.4.1 Façade Construction Recommendations

Based on the predicted façade sound levels shown in **Table 13**, and the threshold criteria outlined in **Table 6**, a detailed building component design analysis is required throughout the proposed development to ensure the indoor sound level criteria is met.

Indoor sound levels, and the building component analysis were completed using the National Research Council's (NRC) Building Practice Note 56 (BPN56). BPN56 is the method for selecting appropriate Sound Transmission Class (STC) ratings for the façade and glazing components to control impacts from transportation noise sources, and satisfy indoor sound level criteria.

Results from an initial building component analysis are shown in **Table 15**. As detailed floor plans were not available at the time of this study, typical unit layouts were assumed based on typical high-rise residential units. It was assumed that living/dining spaces had 70% façade glazing and the sleeping quarters had 50% façade glazing. Overall window STC requirements were determined using the combined (logarithmic addition) requirements from the individual transportation noise impacts from

locomotive, wheel, and roadway noise. STC calculations were completed for daytime and nighttime periods, with the worst-case requirement selected for recommendation. The BPN56 analysis is presented in **Appendix E**. It is recommended that the building component analysis is updated as the development design progresses.

**Table 15: Building Component Analysis**

<b>Building</b>	<b>Required Glazing (STC) Living/Dining Area</b>	<b>Required Glazing (STC) Sleeping Quarters</b>
Tower 1 L2 to L6 North	33	34
Tower 1 L2 to L6 East	39	40
Tower 1 L2 to L6 South	43	43
Tower 1 L7 to L8 North	33	34
Tower 1 L7 to L8 East	39	40
Tower 1 L7 to L8 South	43	44
Tower 1 L7 to L8 West	38	39
Tower 1A L9 to L35 North	34	34
Tower 1A L9 to L35 East	41	42
Tower 1A L9 to L35 South	43	44
Tower 1A L9 to L35 West	38	39
Tower 1B L9 to L35 North	33	34
Tower 1B L9 to L35 East	37	38
Tower 1B L9 to L35 South	40	41
Tower 1B L9 to L35 West	36	37
Tower 2 L2 to L4 North	37	37
Tower 2 L2 to L4 East	32	33
Tower 2 L2 to L4 South	40	40
Tower 2 L2 to L4 West	33	33
Tower 2 L5 to L6 North	34	35
Tower 2 L5 to L6 East	38	39
Tower 2 L5 to L6 South	41	41
Tower 2 L5 to L6 West	34	35



Building	Required Glazing (STC) Living/Dining Area	Required Glazing (STC) Sleeping Quarters
Tower 2A L7 to L35 North	34	34
Tower 2A L7 to L35 East	36	37
Tower 2A L7 to L35 South	35	36
Tower 2A L7 to L35 West	33	33
Tower 2B L7 to L35 North	27	28
Tower 2B L7 to L35 East	39	39
Tower 2B L7 to L35 South	42	43
Tower 2B L7 to L35 West	36	37

The above mentioned STC ratings are conservatively calculated and represent the recommended minimum STC ratings for the windows. Windows should be carefully selected to ensure the entire assembly (frame and glazing) meets the specified minimum STC ratings. It is recommended that manufacturer tests and specifications be reviewed by an Acoustical Consultant upon selection. Sensitive spaces located on corners of buildings, which have multiple façade exposure and potential contribution from multiple sources may require an STC increase of 3.

Additionally, the 24 hour equivalent rail sound level was predicted to be greater than 60 dBA for all sensitive receptors of Tower 1, with the exception of Tower 1 north façade levels 2 to 6, and will require a façade construction of brick veneer or an acoustical equivalent.

As the design progresses, the façade and glazing requirements should be reviewed by an Acoustical Consultant, ideally at the Site Plan Approval (SPA) stage, to confirm or update the above recommended STC ratings.

## 2.3.4.2

**Ventilation Requirements and Warning Clauses**

Based on the predicted sound levels shown in **Table 13** and the threshold criteria outlined in **Table 8**, all residential dwellings of the proposed development require the installation of central air conditioning with a Type D warning clause, as outlined below.

**Type D Warning Clause:** This dwelling unit has been supplied with a central air conditioning system which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the Municipality and the Ministry of the Environment.

Additionally, CN and Metrolinx require that a warning clause regarding the potential for noise and vibration impacts be applied to all sensitive locations within 300 metres of their right-of-way.

**CN Warning Clause:** “Canadian National Railway Company and its assigns or successors in interest has or have a rights-of-way within 1000 metres from the land the subject hereof. There may be alterations to or expansions of the railway facilities on such rights-of-way in the future including the possibility that the railway or its assigns or successors as aforesaid may expand its operations, which expansion may affect the living environment of the residents in the vicinity, notwithstanding the inclusion of any noise and vibration attenuating measures in the design of the development and individual dwelling(s). CN will not be responsible for any complaints or claims arising from use of such facilities and/or operations on, over or under the aforesaid rights-of-way.”

**Metrolinx:** “Metrolinx and its assigns and successors in interest has or have a right-of-way within 300 metres from the land the subject hereof. There may be alterations to or expansions of the rail facilities on such right-of-way in the future including the possibility that Metrolinx or any railway entering into an agreement with Metrolinx to use the right-of-way or their assigns or successors as aforesaid may expand their operations, which expansion may affect the living environment of the residents in the vicinity, notwithstanding the inclusion of any noise and vibration attenuating measures in the design of the development and individual dwelling(s). Metrolinx will not be responsible for any complaints or claims rising from use of such facilities and/or operations on, over or under the aforesaid right-of-way.

The warning clause should be included in agreements that are registered on Title for all Offers of Purchase and Sale, lease/rental agreements, and condominium declarations.

## 2.3.4.3

**Outdoor Living Areas (OLAs)**

As shown in **Table 14**, the sound levels at the amenity terraces are predicted to be in exceedance of the 60 dBA criterion. As such, the outdoor living areas require the installation of noise control measures to achieve predicted levels to 55 dBA, or where not economically feasible, between 55 dBA and 60 dBA and a **Type B** warning clause as outlined below.

**Type B Warning Clause: Purchasers/tenants are advised that despite the inclusion of noise control features in the development and within the building units, sound levels due to increasing road traffic (rail traffic) (air traffic) may on occasions interfere with some activities of the dwelling occupants as the sound levels exceed the sound level limits of the Municipality and the Ministry of the Environment.**

Following MECP's NPC-300, mitigation in the form of acoustic barriers is recommended to reduce the exposure of the outdoor living areas to transportation noise. The following acoustic barriers are recommended to reduce the impacts at the OLAs:

- An acoustic barrier with a height of 2.0 m surrounding the 7<sup>th</sup> floor OLA of Tower 1; and
- An acoustic barrier with a height of 3.0 m surrounding the 5<sup>th</sup> floor OLA of Tower 2.

With the above recommended acoustic barriers, the amenity terraces of the proposed development are predicted to have transportation noise impacts between 55 dBA and 60 dBA. Achieving predicted transportation noise impacts of 55 dBA at the amenity terraces was found to not be feasible with acoustic barriers. Therefore, a Type B warning clause should be applied throughout the proposed development.

The locations and heights of the recommended acoustic barriers are presented in **Figure 4**. The acoustic barriers should have a minimum surface density of 20 kilograms per square metre ( $\text{kg/m}^2$ ). The barriers should be structurally sound, appropriately designed to withstand wind and snow load, and constructed without cracks or surface gaps. Any gaps under the barrier that are necessary for drainage purposes should be minimized and localized, so that the acoustical performance of the barrier is maintained.

The predicted sound levels at the outdoor living areas with the assessed acoustic barrier mitigation are shown in **Table 16**.

**Table 16: Transportation Noise Prediction Summary Table – OLA Impacts with Acoustic Barriers**

<b>Assessment Location</b>	<b>Daytime Equivalent Sound Level - <math>L_{eq}</math> 16-hr (dBA)</b>
Tower 1 – 7 <sup>th</sup> Floor OLA	58
Tower 2 – 5 <sup>th</sup> Floor OLA	59

**2.4****TNM Modelling Confirmation**

Due to the magnitude of noise impacts from Highway 401 on the proposed development, confirmatory noise modelling was completed using STAMSON to demonstrate the accuracy of the TNM protocol. As STAMSON is not capable of incorporating the complex geometries and elevations of the sensitive receptors of the proposed development, the confirmatory modelling was performed on the first story of Building 4 at the closest building setback from the Highway 401.

The confirmatory modelling was completed only considering the Highway 401 noise source.

**Table 17: TNM and STAMSON Confirmatory Modelling**

<b>Assessment Location</b>	<b>TNM Modelling Results</b>	<b>STAMSON Modelling Results</b>
Tower 1 Level 6 South Facade	78.7 dBA	79.6 dBA

As the modelling results for TNM and STAMSON are demonstrated to be within an acceptable range of accuracy, the TNM modelling presented in this study should be considered acceptable.

The STAMSON model has been included in **Appendix D**.

**2.5****Rail Vibration Assessment**

The proposed development is located approximately 30 m from the CN York Subdivision right-of-way. As the proposed development is located within the vibration influence area of 75 m, per the Guidelines for New Development in Proximity to Railway Operations (The Federation of Canadian Municipalities and the Railway Association of Canada, 2013), a vibration assessment for the proposed development is required.

### 2.5.1 Vibration Criteria

There are no MECP guidelines with respect to railway vibration and proposed sensitive land-uses. Applicable guidelines for vibration impacts due to railway operations are those published in the Guidelines for New Development in Proximity to Railway Operations (The Federation of Canadian Municipalities and the Railway Association of Canada, 2013).

Overall vibration levels from railway activities are recommended not to exceed 0.14 millimetres per second (mm/s) root mean square (RMS) in the vertical direction between 4 Hertz (Hz) and 200 Hz, on and above the first floor of all dwellings. This criterion is based on the human perception of ground-borne vibration, published in the International Standard ISO 2631-2. Vibration levels from railway operations meeting this criterion will generally not be perceptible by the occupants.

### 2.5.2 Vibration Measurements

On December 3<sup>rd</sup> and 5<sup>th</sup> 2024, Dillon staff visited the site of the proposed development to conduct field ground vibration measurements at 30 m from the rail right-of-way. Measurements were completed for five freight train passbys. The InstanTel Minimate was used for the field measurements. The instrument can measure peak particle velocity between 2 to 250 Hz. The vertical RMS was then calculated for all train passbys using an averaging time constant of 1 second.

**Table 18** shows the calculated vertical RMS of the five train passbys.

**Table 18: Rail Vibration Measurements**

Date and Time of Rail Passby	Type of Train	Max Vertical RMS (mm/s)	Compliance with Criterion
03/12/24 12:23	Freight	0.054	Yes
03/12/24 12:38	Freight	0.058	Yes
05/12/24 10:50	Freight	0.057	Yes
05/12/24 12:13	Freight	0.050	Yes
05/12/24 13:45	Freight	0.046	Yes

The location of rail vibration measurements has been shown in **Figure 5**. Two vibration monitors were utilized for measurements. The results shown in **Table 18** represent the maximum vertical RMS calculated between each unit. The monitoring locations were changed between December 3<sup>rd</sup> and December 5<sup>th</sup> based on accessibility to the site. The measured ground vibration levels from train passbys were found to be below the applicable criteria. As such, mitigation measures are not predicted to be required.

## 3.0

## Impacts from the Proposed Development on itself and the Environment

The mechanical equipment of the proposed development should be assessed for noise impacts on the proposed development itself and the surrounding environment. At the time of this assessment, the mechanical plans for the proposed development were not available.

The future mechanical equipment of the proposed development should be located to reduce exposure to the receptors of the proposed development and the surrounding environment and where possible should be located within mechanical penthouses. Where isolation from noise sensitive receptors is not possible, equipment selection should be completed with consideration for reducing the noise emissions of the equipment.

As mechanical plans become available for the proposed development, it is Dillon's recommendation that a qualified acoustic consultant assesses the stationary noise impacts of the equipment on the development itself and the surrounding environment.

## Conclusions

Dillon Consulting Limited (Dillon) was retained by 1095 Kingston Road Ltd. C/O Resident to complete a noise and vibration assessment for a proposed development. This study has been completed in support of the submission application for the proposed development.

The noise assessment presented herein focuses on the noise impacts of nearby stationary noise sources and transportation corridors on the proposed development.

The noise assessment was prepared in accordance with the requirements of the Region of Durham and that of the Ontario Ministry of Environment, Conservation and Parks (MECP) noise publication NPC-300. Based on the results of the completed study, the following conclusions have been reached:

As outlined in **Section 2.1**, stationary noise impacts on the proposed development are predicted to be in compliance with applicable noise criteria.

As outlined in **Section 2.3**, transportation noise impacts on the proposed development can be sufficiently controlled by:

- The installation of central air conditioning with a Type D warning clause;
- Upgraded window glazing;
- Façade construction of brick veneer or an acoustical equivalent; and
- Installation of acoustic barriers with a Type B warning clause.

As outlined in **Section 2.5**, rail vibration impacts on the proposed development are predicted to be in compliance with applicable vibration criteria.

Due to the proximity to CN York Subdivision, CN Kingston Subdivision, and GO Transit Lakeshore East Subdivision, CN and Metrolinx require that warning clauses be applied to the proposed development.

As the design of the development progresses and building orientations, elevations, ground contours, and detailed building plans are finalized, this assessment should be updated by an Acoustic Consultant.



## 5.0

## Closure

This noise and vibration assessment has been prepared based on the information provided and/or approved by 1095 Kingston Road Ltd. C/O Resident. This report is intended to provide a reasonable review of available information within an agreed work scope, schedule, and budget. This report was prepared by Dillon for the sole benefit of 1095 Kingston Road Ltd. C/O Resident. The material in the report reflects Dillon's judgement in light of the information available to Dillon at the time of this report preparation. Any use which a third party makes of this report, or any reliance on or decisions made based on it, are the responsibilities of such third parties. Dillon accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this report.

We trust that the report is to your satisfaction. Please do not hesitate to contact the undersigned if you have any further questions on this report.

Respectfully Submitted:

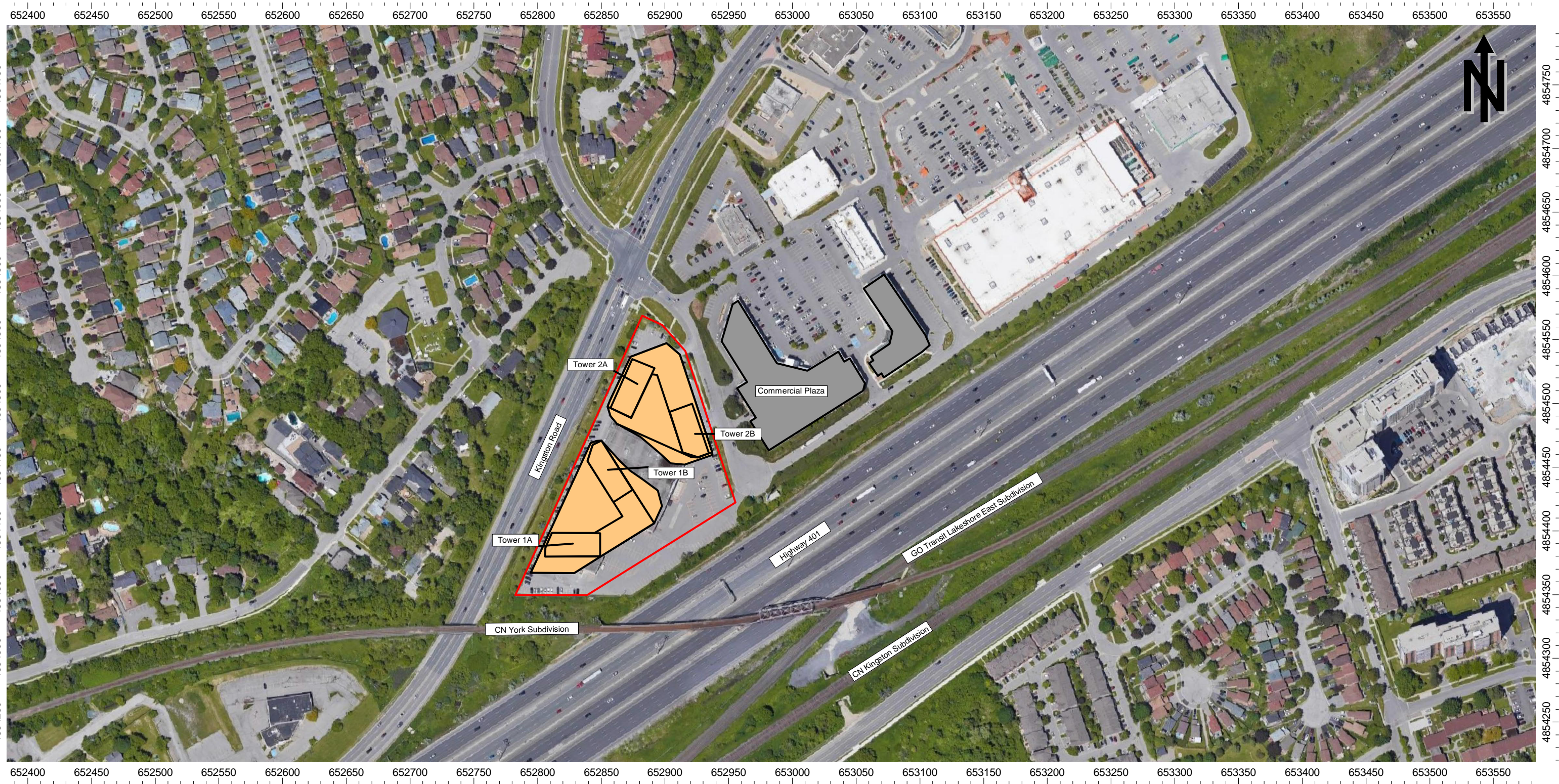
**Dillon Consulting Limited**



Callum Heggart, P. Eng

## Figures





**Figure 1**

Project # 24-9327

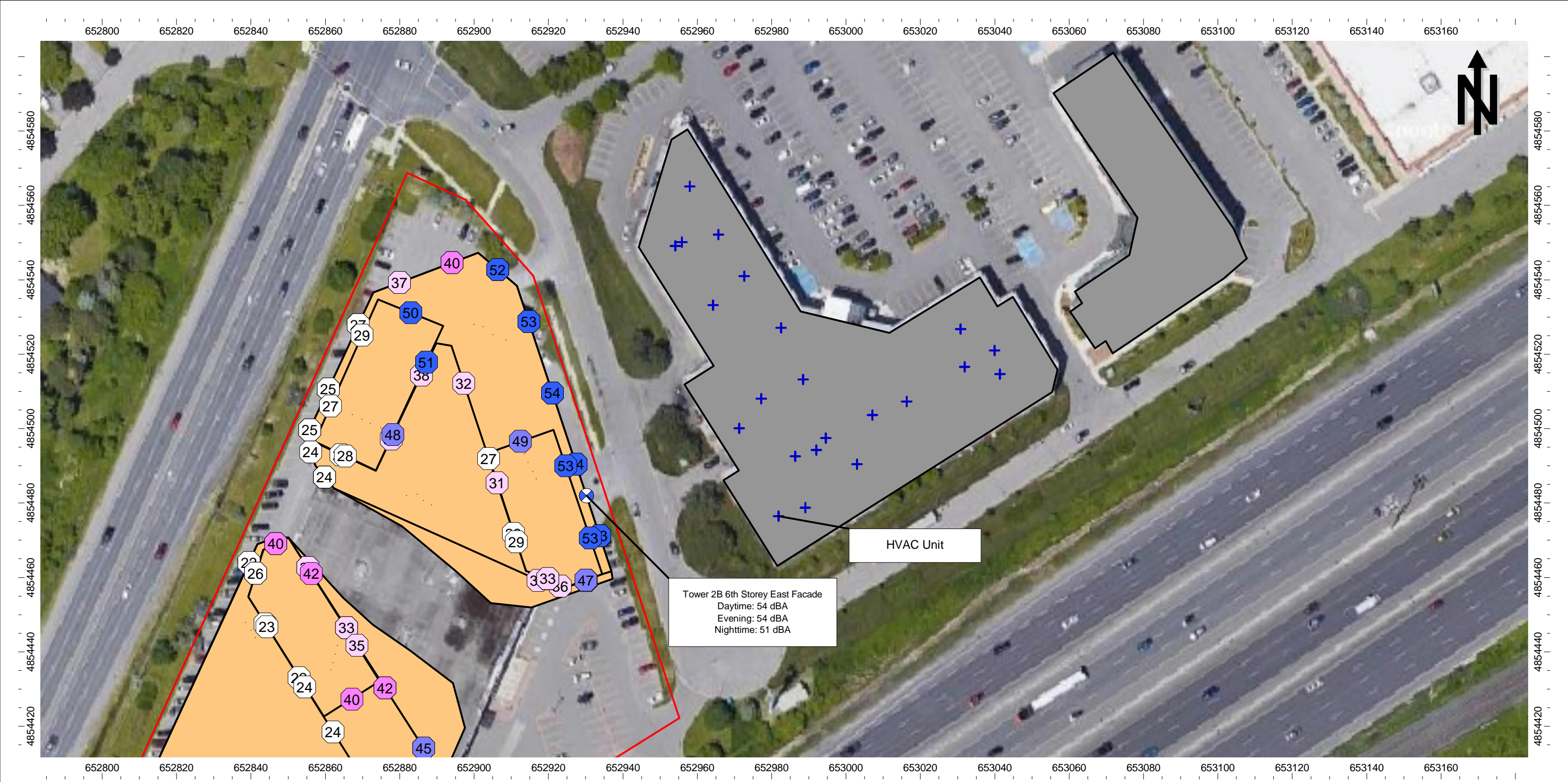
Feb 2025

## Subject Site and Surrounding Area

1095 Kingston Road, Pickering, Ontario







**Figure 2**

Project # 24-9327

Feb 2025





**Figure 3**

Project # 24-9327

Feb 2025

## Predicted Transportation Noise Impacts - Daytime



1095 Kingston Road, Pickering, Ontario





**Figure 4**

Project # 24-9327

Feb 2025

## Predicted Transportation Noise Impacts Mitigated Outdoor Living Areas

1095 Kingston Road, Pickering, Ontario







**Figure 5**

Project # 24-9327

Feb 2025

**Vibration Monitoring Locations**



## Appendix A

### Development Site Plan



# BDP. Quadrangle

**Quadrangle Architects Limited**  
The Well, 8 Spadina Avenue, Suite 2100, Toronto, ON M5V 0S8  
t 416 598 1240 www.bdpquadrangle.com

## 1095 Kingston Road, Pickering

Ontario, Canada

for  
Resident

Project No. 21068  
Date MAR 2025  
Issued for ZBA SUBMISSION (DRAFT)

### ARCHITECTURAL DRAWINGS

A000.S Cover Page  
A001.S Statistics  
A101.S Site Plan  
A103.S PT Underground  
A201.S Ground Floor Plan  
A202.S Mezzanine Floor Plan  
A203.S Level 2 Floor Plan  
A204.S Level 3rd Floor Plan  
A205.S Level 5 Floor Plan  
A206.S Level 6 Floor Plan  
A207.S Level 7 & 8 Floor Plan  
A208.S Level 9 Floor Plan  
A210.S Typical Tower Floor Plan  
A211.S MPH Floor Plan  
A212.S Roof Plan  
A401.S Building Elevations  
A402.S Building Elevations  
A451.S Building Section  
A452.S Building Section  
A453.S Building Section

#### PLANNING CONSULTANT

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24722 Kingston Road  
Toronto, ON M1N 1V3  
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8395 Jane Street  
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#### LANDSCAPE ARCHITECT

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#### TRAFFIC CONSULTANT

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T: 416.961.7110

#### WIND CONSULTANT

Gnobl Consulting Inc.  
N/A  
Guelph, ON  
T: 226.343.0728

#### GEOTECHNICAL & ENVIRONMENTAL ENGINEER

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#### NOISE & VIBRATION CONSULTANT

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Suite 301  
Guelph, ON, N1H 3N4  
T: 519.571.9633

C:\Users\ML4239\Documents\BDO\_P01\_1096\_Kingston Road\_2025\_ML4239.rvt

		Floor	GBA/Typ. Floor (sqm)	No. Typ. Floors	GBA Gross Building Area (sqm excl. balconies)		Exemptions	City Centre By-law T88(17) Net Floor Area (sqm)		Number of Units							
					sqm	sf		sqm	sf	B	1B	1B+D	2B	2B+D	3B	Total Units	
PHASE 1 / BUILDING 1 TWO 35-STORY TOWERS + 8-STORY PODIUM	TOWER 1B	MPH	750	1	750	8,073	750	0	MPH								
		Level 10-35	750	26	15,500	209,898	1,403	18,098	194,813	Level 10-35		130	52	52	26	26	288
		Level 6	750	1	750	8,073	54	696	7,493	Level 6		5	2	1	1	0	9
	TOWER 1A	MPH	750	4	750	8,073	750	0	MPH								
		Level 10-35	750	26	15,500	209,898	1,403	18,098	194,813	Level 10-35		104	78	52	26	26	288
		Level 6	750	1	750	8,073	54	696	7,493	Level 6		4	0	0	0	0	4
	PODIUM	Level 6	2,509	1	2,509	27,207	181	2,138	25,059	Level 6		11	20	2	2	3	38
		Level 7	2,509	1	2,509	27,207	507	2,402	25,855	Level 7		11	16	2	2	3	38
		Level 8	2,509	1	2,509	27,207	507	2,402	25,855	Level 8		11	16	2	2	3	38
		Level Mezz	3,754	1	3,754	40,420	3,633	3,321	3,396	Level Mezz						0	60
Ground Floor		5,306	1	5,306	57,447	3,362	5,367	58,069	Ground Floor					1	0	10	
Building 1 Total			34		60,592	637,503		68,736	734,673					147	57	727	
BUILDING HEIGHT																	
Building height			114.36m														
Height to top of MPH roof			120.36m														



SURVEYOR'S REAL PROPERTY REPORT  
PART 1 - PLAN OF SURVEY AND  
TOPOGRAPHY OF  
PART OF LOT 25  
CONCESSION 1  
(GEOGRAPHIC TOWNSHIP OF PICKERING)  
CITY OF PICKERING  
REGIONAL MUNICIPALITY OF DURHAM

SCALE 1:200

HOLDING JONES VANDERVEEN INC.  
ONTARIO LAND SURVEYORS

METRES

HEIGHTS AND ELEVATIONS SHOWN ON THIS PLAN ARE IN METRES  
AND CAN BE CONVERSED TO FEET BY DIVIDING BY 0.3048

PART 2 - REPORT

THIS PLAN COMPRISES ALL OF PPM 26037-0068.

REGULATORY COMPLIANCE REQUIREMENTS

SUBJECT TO AN EASEMENT OVER PART 1, 400-2042 AS IN PART 1, 400-2042  
SUBJECT TO EASEMENT OVER PART 1, 400-2042 AS IN PART 1, 400-2042

PARTIALLY RELEASED OVER PART 1, 400-2042 AS IN PART 1, 400-2042

DISCLAIMER

NOTE THAT CURRENT EXTENTS OUTSIDE OF THE PARCEL UNITS IN THE MOST SOUTH-WESTERLY CORNER  
NOTE THAT EXTENTS OF ADJACENT PARCELS (OWNED) REGISTRATION PLAN P-2300-102, REGISTERED IN 1971 AS  
NOTE THAT EXTENTS OF ADJACENT PARCELS (OWNED) REGISTRATION PLAN P-2300-102, REGISTERED IN 1971 AS  
NOTE THAT EXTENTS OF ADJACENT PARCELS (OWNED) REGISTRATION PLAN P-2300-102, REGISTERED IN 1971 AS

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SITE PLAN LEGEND

PROPERTY LINE	LINE OF UNDERGROUND GARAGE BELOW
MAIN BUILDING ENTRANCE	EXIT
VEHICLE / LOADING ENTRANCE / EXIT	FIRE HYDRANT
SIAMSE CONNECTION	MANHOLE COVER
AREA DRAIN	CATCH BASIN
FLOOR DRAIN (PARKING SLAB)	FLOOR DRAIN (INTERIOR)
EXISTING LIGHT	FINISH FLOOR ELEVATION
EXISTING ELEVATION	PROPOSED ELEVATION
TOP OF ROOF	FIRE ACCESS ROUTE HEAVY DUTY PAVING
ASSEMBLY TO BE DESIGNED TO MEET THE LOADS IMPOSED BY FIRE FIGHTING EQUIPMENT	OUTDOOR AMENITY
GREEN ROOF	

Date	No.	Description
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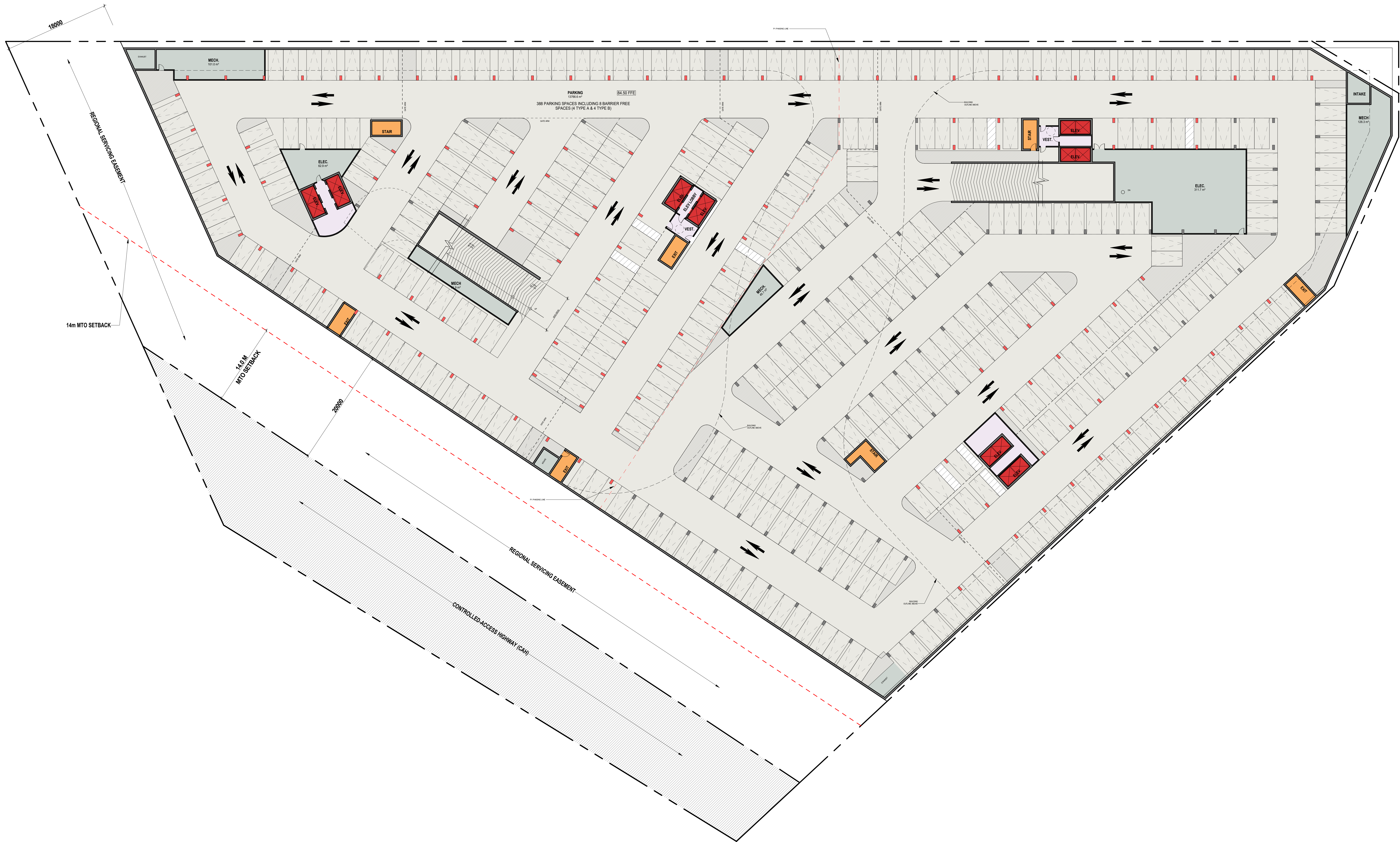
21068 300 ML SR  
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Site Plan

A101.S

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**PARKING NOTES:**

1. MINIMUM PARKING SPACE SIZES (UNLESS OTHERWISE NOTED):
  - 3000mm WIDE X 5000mm LONG (NO SIDES OBSTRUCTED)
  - 2000mm WIDE X 5000mm LONG (ONE SIDE OBSTRUCTED)
  - 3000mm WIDE X 5000mm LONG (TWO SIDES OBSTRUCTED)
2. MAINTAIN MINIMUM DRIVEABLE WIDTH OF 6000mm UNLESS OTHERWISE NOTED.
3. MAINTAIN MINIMUM HEADROOM CLEARANCE OF 2100mm THROUGHOUT.

**PARKING LEGEND:**

- COMMERCIAL PARKING SPACE
- RESIDENTIAL PARKING SPACE
- VISITOR PARKING SPACE
- EXISTING PARKING SPACE
- BIKE LOCKER
- BIKE PARKING (STACKED)
- BIKE PARKING (VERTICAL)
- CONVEX MIRROR
- ELECTRIC VEHICLE
- LIGHT STANDARD
- PAINTED LINES
- FIRE-RATED BULKHEAD

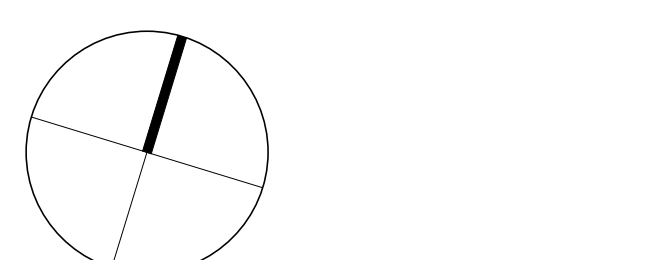
**PARKING DIMENSIONS:**

- TYPICAL: 3000 x 5000
- ONE SIDE OBSTRUCTED: 2000 x 5000
- PARALLEL PARKING: 2000 x 5000
- ACCESSIBLE VISITOR - TYPE A: 3000 x 5000
- ACCESSIBLE VISITOR - TYPE B: 3000 x 5000

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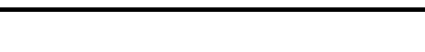
21068 250 ML/ME/JK SR  
PROJECT SCALE DRAWN REVIEWED

P1 Underground

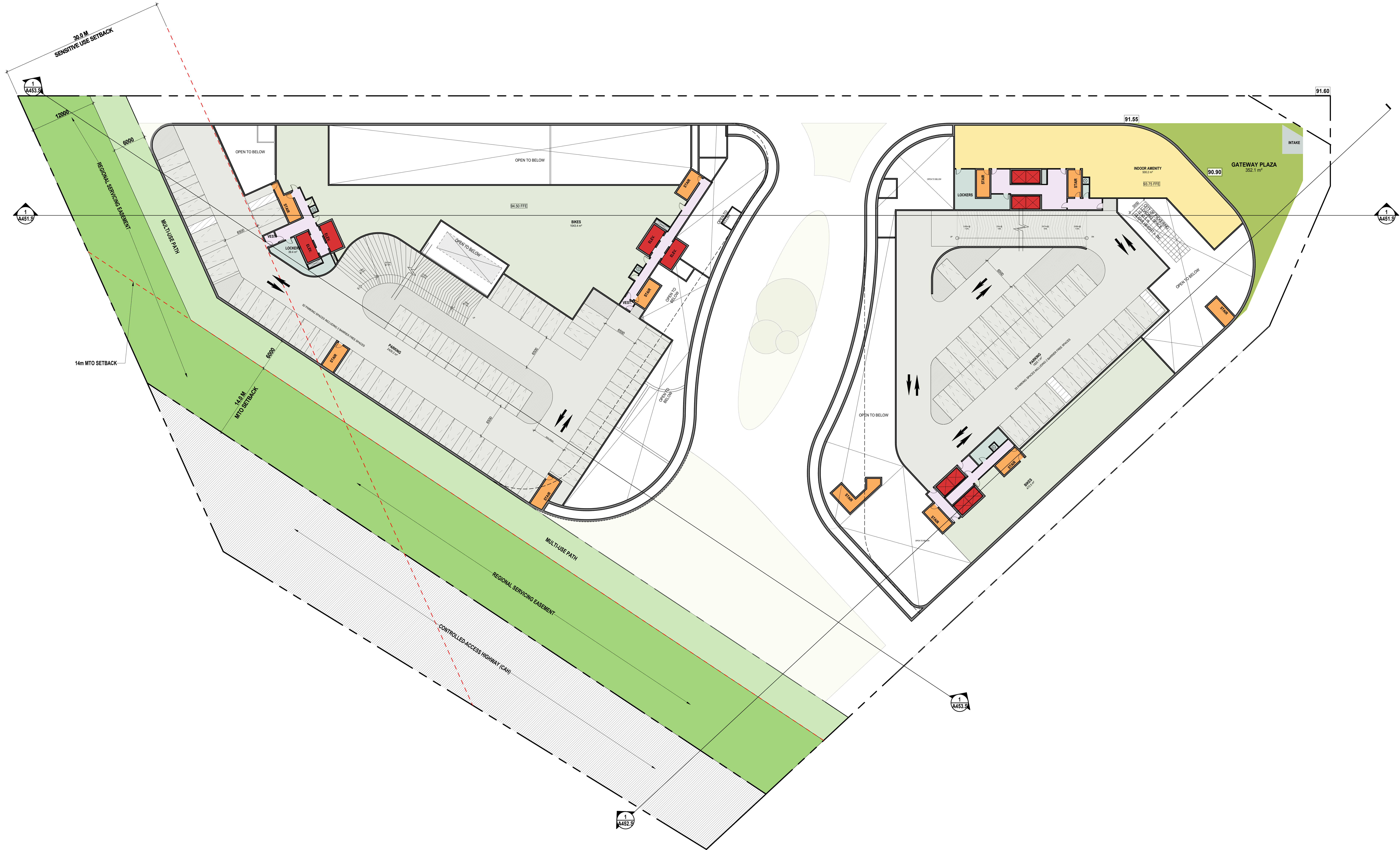
**A103.S**

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- 3000mm WIDE X 5000mm LONG (TWO SIDES OBSTRUCTED)

2. MAINTAIN MINIMUM DRIVEABLE WIDTH OF 6000mm UNLESS OTHERWISE NOTED.

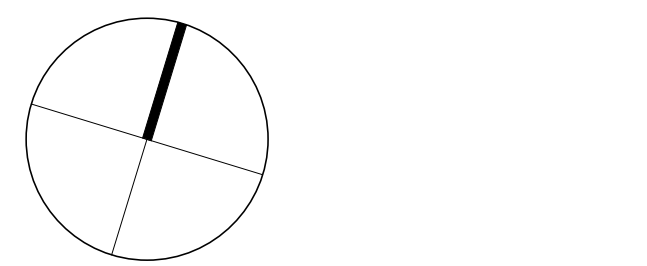
3. MAINTAIN MINIMUM HEADROOM CLEARANCE OF 2100mm THROUGHOUT.

- PARKING LEGEND:**
- COMMERCIAL PARKING SPACE
  - RESIDENTIAL PARKING SPACE
  - VISITOR PARKING SPACE
  - EXISTING PARKING SPACE
  - BIKE LOCKER
  - BIKE PARKING (STACKED)
  - BIKE PARKING (VERTICAL)
  - CONVEX MIRROR
  - ELECTRIC VEHICLE
  - LIGHT STANDARD
  - PAINTED LINES
  - FIRE-RATED BULKHEAD
- Typical dimensions for parking spaces:
- TYPICAL: 3000mm x 5000mm
  - ONE SIDE OBSTRUCTED: 2000mm x 5000mm
  - PARALLEL PARKING: 3000mm x 5000mm
  - ACCESSIBLE VISITOR - TYPE A: 3000mm x 5000mm
  - ACCESSIBLE VISITOR - TYPE B: 3000mm x 5000mm

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Mezzanine Floor Plan

**A202.S**

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**PARKING NOTES:**

1. MINIMUM PARKING SPACE SIZES (UNLESS OTHERWISE NOTED):

- 3000mm WIDE X 5000mm LONG (NO SIDES OBSTRUCTED)
- 2000mm WIDE X 5000mm LONG (ONE SIDE OBSTRUCTED)
- 3000mm WIDE X 5000mm LONG (TWO SIDES OBSTRUCTED)

2. MAINTAIN MINIMUM DRIVEABLE WIDTH OF 6000mm UNLESS OTHERWISE NOTED.

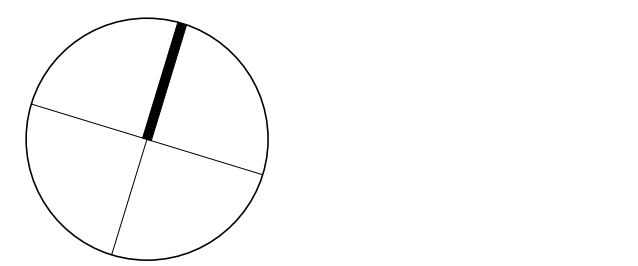
3. MAINTAIN MINIMUM HEADROOM CLEARANCE OF 2100mm THROUGHOUT.

- PARKING LEGEND:**
- COMMERCIAL PARKING SPACE
  - RESIDENTIAL PARKING SPACE
  - VISITOR PARKING SPACE
  - EXISTING PARKING SPACE
  - BIKE LOCKER
  - BIKE PARKING (STACKED)
  - BIKE PARKING (VERTICAL)
  - CONVEX MIRROR
  - ELECTRIC VEHICLE
  - LIGHT STANDARD
  - PAINTED LINES
  - FIRE-RATED BULKHEAD
- TYPICAL
- ONE SIDE OBSTRUCTED
- PARALLEL PARKING
- ACCESSIBLE VISITOR - TYPE A
- ACCESSIBLE VISITOR - TYPE B

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Level 2 Floor Plan

**A203.S**

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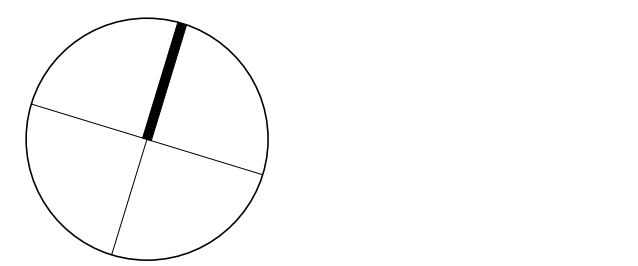
- PARKING NOTES:**
1. MINIMUM PARKING SPACE SIZES (UNLESS OTHERWISE NOTED):
    - 3000mm WIDE X 5000mm LONG (NO SIDES OBSTRUCTED)
    - 2000mm WIDE X 5000mm LONG (ONE SIDE OBSTRUCTED)
    - 3000mm WIDE X 5000mm LONG (TWO SIDES OBSTRUCTED)
  2. MAINTAIN MINIMUM DRIVEABLE WIDTH OF 6000mm UNLESS OTHERWISE NOTED.
  3. MAINTAIN MINIMUM HEADROOM CLEARANCE OF 2100mm THROUGHOUT.

- PARKING LEGEND:**
- COMMERCIAL PARKING SPACE
  - RESIDENTIAL PARKING SPACE
  - VISITOR PARKING SPACE
  - EXISTING PARKING SPACE
  - BIKE LOCKER
  - BIKE PARKING (STACKED)
  - BIKE PARKING (VERTICAL)
  - CONVEX MIRROR
  - ELECTRIC VEHICLE
  - LIGHT STANDARD
  - PAINTED LINES
  - FIRE-RATED BULKHEAD
- Typical dimensions for parking spaces and setbacks are shown with diagrams:
- TYPICAL: 3000 x 5000
  - ONE SIDE OBSTRUCTED: 2000 x 5000
  - PARALLEL PARKING: 3000 x 5000
  - ACCESSIBLE VISITOR - TYPE A: 3000 x 5000
  - ACCESSIBLE VISITOR - TYPE B: 3000 x 5000

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Level 3-4 Floor Plan

A204.S

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- 3000mm WIDE X 5000mm LONG (TWO SIDES OBSTRUCTED)

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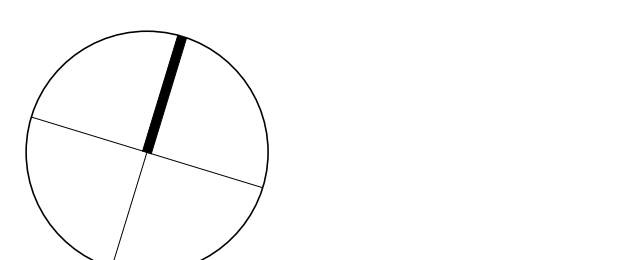
3. MAINTAIN MINIMUM HEADROOM CLEARANCE OF 2100mm THROUGHOUT.

- PARKING LEGEND:**
- COMMERCIAL PARKING SPACE
  - RESIDENTIAL PARKING SPACE
  - VISITOR PARKING SPACE
  - EXISTING PARKING SPACE
  - BIKE LOCKER
  - BIKE PARKING (STACKED)
  - BIKE PARKING (VERTICAL)
  - CONVEX MIRROR
  - ELECTRIC VEHICLE
  - LIGHT STANDARD
  - PAINTED LINES
  - FIRE-RATED BULKHEAD
- TYPICAL
- ONE SIDE OBSTRUCTED
- PARALLEL PARKING
- ACCESSIBLE VISITOR - TYPE A
- ACCESSIBLE VISITOR - TYPE B

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Level 5 Floor Plan

A205.S

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  - 3000mm WIDE X 5000mm LONG (TWO SIDES OBSTRUCTED)
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3. MAINTAIN MINIMUM HEADROOM CLEARANCE OF 2100mm THROUGHOUT.

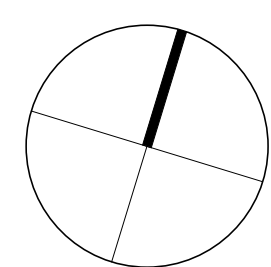
**PARKING LEGEND:**

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  - RESIDENTIAL PARKING SPACE
  - VISITOR PARKING SPACE
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  - BIKE LOCKER
  - BIKE PARKING (STACKED)
  - BIKE PARKING (VERTICAL)
  - CONVEX MIRROR
  - ELECTRIC VEHICLE
  - LIGHT STANDARD
  - PAINTED LINES
  - FIRE-RATED BULKHEAD
- TYPICAL  
ONE SIDE OBSTRUCTED  
PARALLEL PARKING  
ACCESSIBLE VISITOR - TYPE A  
ACCESSIBLE VISITOR - TYPE B

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Level 6 Floor Plan

**A206.S**

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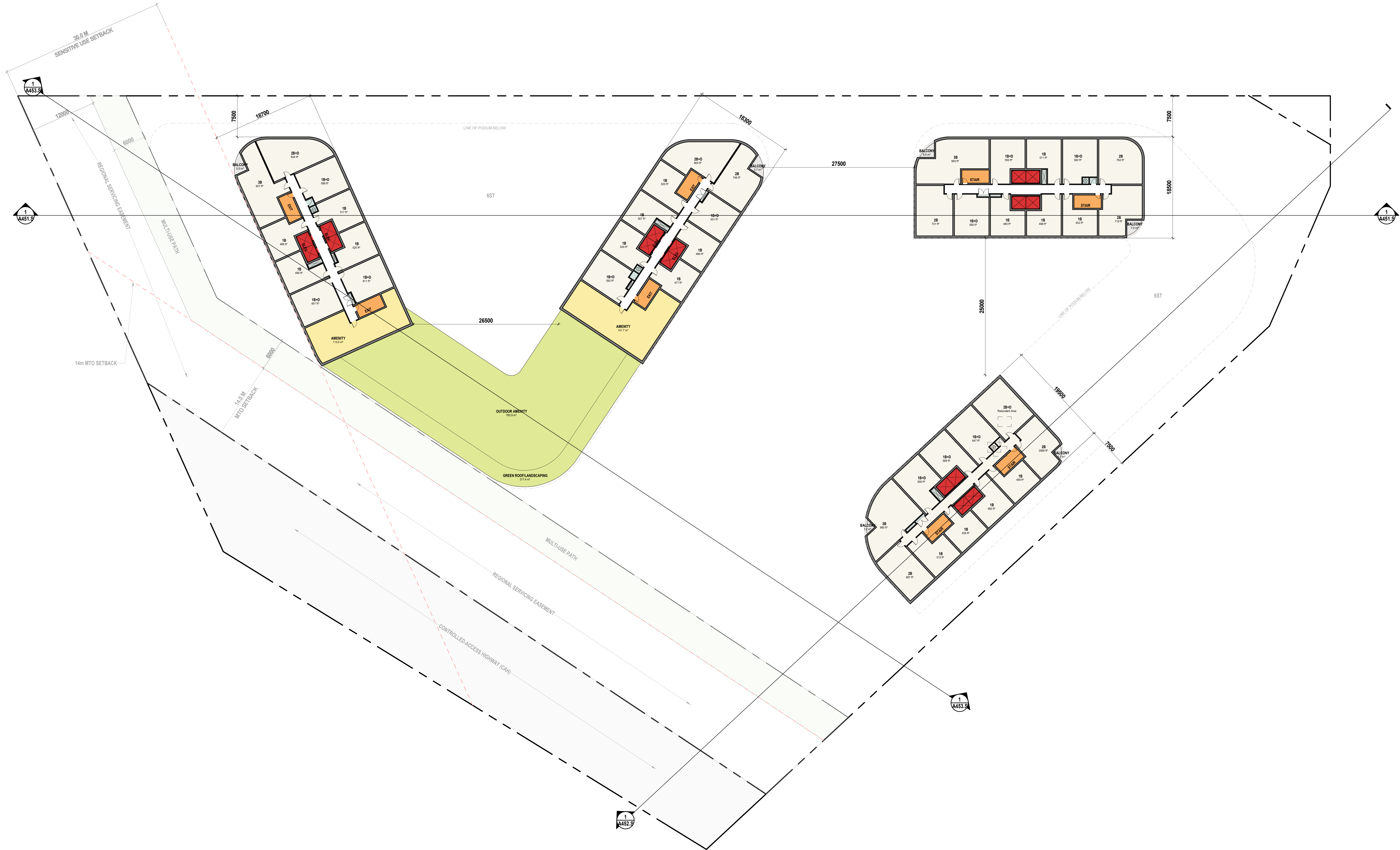
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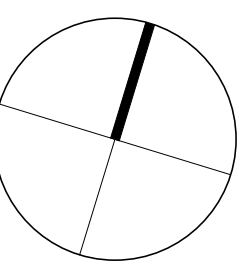




Date	No.	Description
REVISION RECORD		

DRAFT

MAR 2025	ZBA Submission
ISSUE RECORD	



**BDP.**  
**Quadrangle**

Quadrangle Architects Limited  
The West, 8 Spadina Avenue, Suite 2100, Toronto, ON M5V 0S8  
1 416 598 1240 www.bdpquadrangle.com

1095 Kingston Road, Pickering  
Ontario, Canada  
for  
Resident

21068 1 : 250 ML/ME/JK SR  
PROJECT SCALE DRAWN REVIEWED

Level 9 Floor Plan

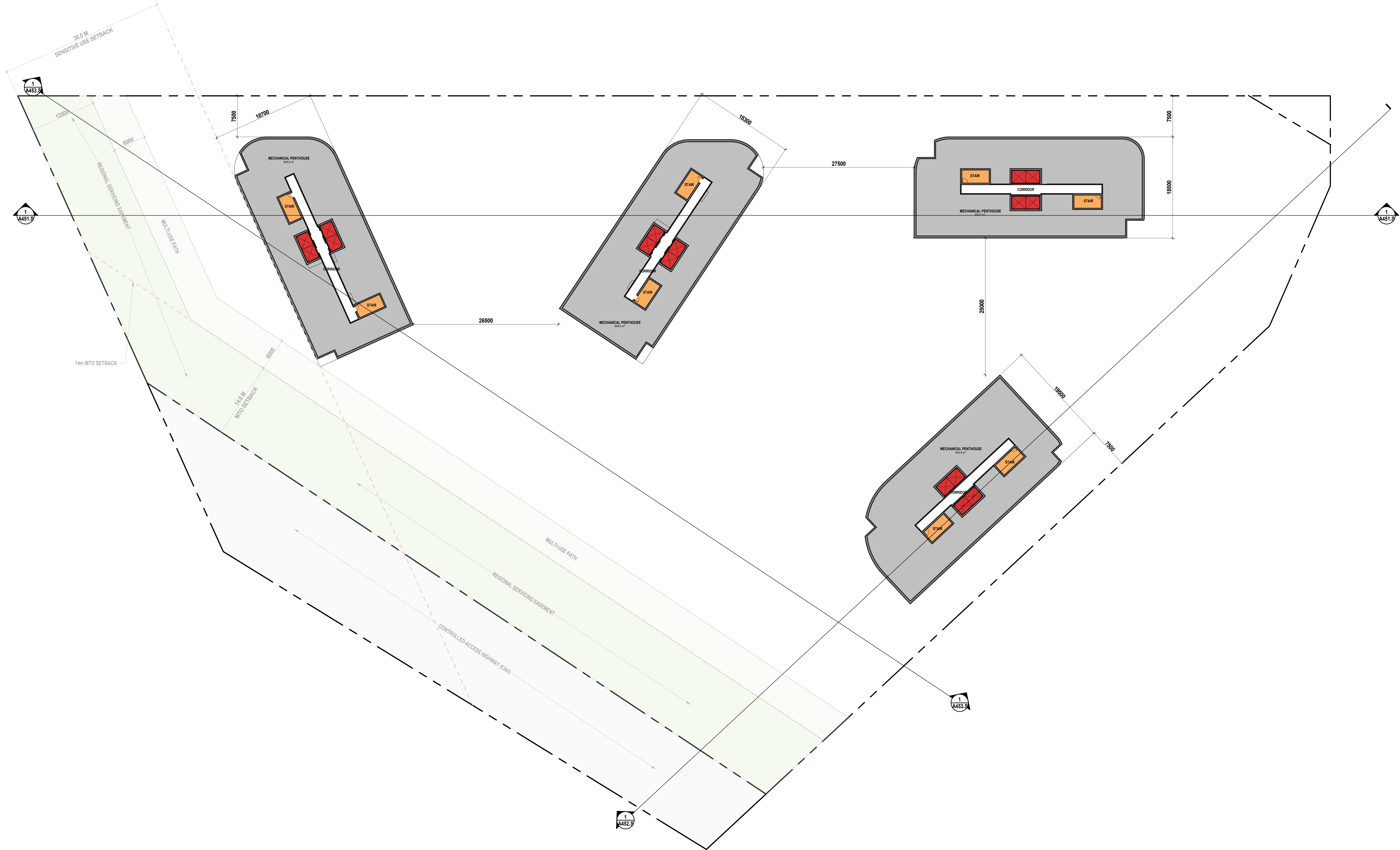
**A209.S**

Note: This drawing is the property of the Architect and may not be reproduced or used without the express consent of the Architect. The Contractor is responsible for checking and verifying all levels and dimensions and shall report all discrepancies to the Architect and obtain clarification prior to commencing work.





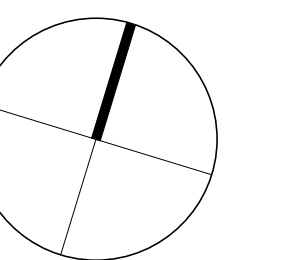




Date	No.	Description
REVISION RECORD		

DRAFT

MAR 2025	ZBA Submission
ISSUE RECORD	



**BDP.**  
**Quadrangle**

Quadrangle Architects Limited  
The West, 8 Spadina Avenue, Suite 2100, Toronto, ON M5V 0S8  
1 416 598 1240 - www.bdpquadrangle.com

1095 Kingston Road, Pickering  
Ontario, Canada  
for  
Resident

21068 1 : 250 ML/ME/JK SR  
PROJECT SCALE DRAWN REVIEWED

MPH Floor Plan

**A211.S**

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MAR 2025	ZBA Submission
ISSUE RECORD	

## BDP. Quadrangle

**Quadrangle Architects Limited**  
The Well, 8 Spadina Avenue, Suite 2100, Toronto, ON M5V 0S8  
t 416 598 1240 www.bdpquadrangle.com

1095 Kingston Road, Pickering  
Ontario, Canada  
for  
Resident

21068 1 : 250 ML/ME/JK SR  
PROJECT SCALE DRAWN REVIEWED

A451.S

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1/1



## Appendix B

### D-6 Classification Criteria

Category	Outputs	Scale	Process	Operations/Intensity	Possible Examples
Class I	<ul style="list-style-type: none"><li>• Noise: Sound not audible off property</li><li>• Dust and/or Odour: Infrequent and not intense</li><li>• Vibration: No ground borne vibration on plant property</li></ul>	<ul style="list-style-type: none"><li>• No outside storage</li><li>• Small scale plant or scale is irrelevant in relation to all other criteria for this Class</li></ul>	<ul style="list-style-type: none"><li>• Self-contained plant or building which produces/stores a packaged product. Low probability of fugitive emissions</li></ul>	<ul style="list-style-type: none"><li>• Daytime operations only</li><li>• Infrequent movement of products and/or heavy trucks</li></ul>	<ul style="list-style-type: none"><li>• Electronics manufacturing and repair</li><li>• Furniture repair and refinishing</li><li>• Beverages bottling</li><li>• Auto parts supply</li><li>• Packaging and crafting services</li><li>• Distribution of dairy products</li><li>• Laundry and linen supply</li></ul>
Class II	<ul style="list-style-type: none"><li>• Noise: Sound occasionally audible off property</li><li>• Dust and/or Odour: Frequent and occasionally intense</li><li>• Vibration: Possible groundborne vibration, but cannot be perceived off property</li></ul>	<ul style="list-style-type: none"><li>• Outside storage permitted</li><li>• Medium level of production allowed</li></ul>	<ul style="list-style-type: none"><li>• Open process</li><li>• Periodic outputs of minor annoyance</li><li>• Low probability of fugitive emissions</li></ul>	<ul style="list-style-type: none"><li>• Shift operations permitted</li><li>• Frequent movement of products and/or heavy trucks with the majority of movements during daytime hours</li></ul>	<ul style="list-style-type: none"><li>• Magazine printing</li><li>• Paint spray booths</li><li>• Metal command</li><li>• Electrical production manufacturing</li><li>• Manufacturing of dairy products</li><li>• Dry cleaning services</li><li>• Feed packing plant</li></ul>
Class III	<ul style="list-style-type: none"><li>• Noise: sound frequently audible off property</li><li>• Dust and/or Odour: Persistent and/or intense</li><li>• Vibration: Ground-borne vibration can frequently be perceived off property</li></ul>	<ul style="list-style-type: none"><li>• Outside storage of raw and finished products</li><li>• Large production levels</li></ul>	<ul style="list-style-type: none"><li>• Open process</li><li>• Frequent outputs of major annoyances</li><li>• High probability of fugitive emissions</li></ul>	<ul style="list-style-type: none"><li>• Continuous movement of products and employees</li><li>• Daily shift operations permitted</li></ul>	<ul style="list-style-type: none"><li>• Manufacturing of paint and varnish</li><li>• Organic chemicals manufacturing</li><li>• Breweries</li><li>• Solvent recovery plants</li><li>• Soaps and detergent manufacturing</li><li>• Manufacturing of resins and costing</li><li>• Metal manufacturing</li></ul>

## Appendix C

### Traffic Data



Heggart, Callum <cheggart@dillon.ca>

Road traffic information request

2 messages

Heggart, Callum <cheggart@dillon.ca>

Thu, Dec 12, 2024 at 10:18 AM

To: noiserequests@durham.ca


Hi,

I am completing a transportation noise study for a proposed development located at 1095 Kingston Road in Pickering Ontario.

Can you please provide the following information for Kingston Road in proximity to 1095 Kingston Road:

- Forecasted AADT and SADT
- Percentage of medium and heavy trucks

Please note that I have recently completed a study at 705 Kingston Road in Pickering and used the following information for Kingston Road. Please let me know if that data is valid for 1095 Kingston Road as well.



The Regional Municipality of Durham

---

**ROAD SEGMENT TRAFFIC FORECASTS FOR NOISE ANALYSES**

This information is to be used as the basis for assessing the potential impacts of noise, generated by traffic on Provincial Highways and arterial roads, on proposed land uses that are sensitive (e.g., residential subdivisions). Arterial roads include existing and future Type A, B and C, as designated in the Durham Regional Official Plan.

Noise assessment reports recommend specific measures to be integrated into the design of sensitive developments to reduce road noise impacts to acceptable levels.

Planning and Economic Development Department

Planning Division

605 ROSSLAND RD. E.  
4TH FLOOR  
P.O. BOX 623  
WHITBY, ON L1N 6A3  
CANADA  
905-668-7711  
1-800-372-1102  
Fax: 905-666-6208  
E-Mail: [planning@durham.ca](mailto:planning@durham.ca)

[www.durham.ca](http://www.durham.ca)

**Brian Bridgeman, MCIP, RPP, PLE**  
Commissioner of Planning and Economic Development

**Provided For:**

Name / Name of Firm: Callie Airdrie, Dillon Consulting Ltd

Address: 51 Breithaupt Street, Suite 200, Kitchener, ON N2H 5G5

Telephone: (519) 571-9833 Fax:

**Location of Proposal:**

705 Kingston Road, Pickering

Municipality: Lot(s): Concession:

Durham Region File No. (if available):

Name of Property Owner (if available):

**Date Request Received:** September 28, 2024 **Received By:** Anthony Caruso

**Date Forecast Sent:** October 4, 2024

Name of Road Segment	Forecasted AADT*	No. of Lanes	% of Trucks	Heavy : Medium Truck Ratio	Speed (km/h)
Kingston Road (Whites to Fairport)	35,000	4	8	30 70	60
Whites Road (Kingston to Sheppard)	35,000	6	10	70 30	60

\* Average Annual Daily Traffic. Forecast based on ultimate development according to the Durham Regional Official Plan.

Thanks  
Callum



**Callum Heggart**  
**Dillon Consulting Limited**  
Suite 200 - 51 Breithaupt Street  
Kitchener, Ontario, N2H 5G5  
C - 519.577.7832  
T - 519.571.9833 ext. 3153  
[CHeggart@dillon.ca](mailto:CHeggart@dillon.ca)  
[www.dillon.ca](http://www.dillon.ca)

---

**noiserequests** <[noiserequests@durham.ca](mailto:noiserequests@durham.ca)>  
To: "Heggart, Callum" <[cheggart@dillon.ca](mailto:cheggart@dillon.ca)>

Thu, Dec 19, 2024 at 1:17 PM

Hi Callum,

The data is the same at 705 and [1095 Kingston Road](#).

Thank you,

Anthony

---

**From:** Heggart, Callum <[cheggart@dillon.ca](mailto:cheggart@dillon.ca)>  
**Sent:** Thursday, December 12, 2024 10:19 AM  
**To:** noiserequests <[noiserequests@durham.ca](mailto:noiserequests@durham.ca)>  
**Subject:** Road traffic information request

You don't often get email from [cheggart@dillon.ca](mailto:cheggart@dillon.ca). [Learn why this is important](#)

Hi,

I am completing a transportation noise study for a proposed development located at [1095 Kingston Road](#) in Pickering Ontario.

Can you please provide the following information for Kingston Road in proximity to [1095 Kingston Road](#):

- Forecasted AADT and SADT
- Percentage of medium and heavy trucks

Please note that I have recently completed a study at [705 Kingston Road](#) in Pickering and used the following information for Kingston Road. Please let me know if that data is valid for [1095 Kingston Road](#) as well.



## The Regional Municipality of Durham

Planning and Economic  
Development Department

Planning Division

605 ROSSLAND RD. E.  
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P.O. BOX 623  
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[www.durham.ca](http://www.durham.ca)

**Brian Bridgeman, MCIP, RPP, PLE**  
Commissioner of Planning and  
Economic Development

### ROAD SEGMENT TRAFFIC FORECASTS FOR NOISE ANALYSES

This information is to be used as the basis for assessing the potential impacts of noise, generated by traffic on Provincial Highways and arterial roads, on proposed land uses that are sensitive (e.g., residential subdivisions). Arterial roads include existing and future Type A, B and C, as designated in the Durham Regional Official Plan.

Noise assessment reports recommend specific measures to be integrated into the design of sensitive developments to reduce road noise impacts to acceptable levels.

#### Provided For:

Name / Name of Firm: Collie Airdrie, Dillon Consulting Ltd  
Address: 51 Breithaupt Street, Suite 200, Kitchener, ON N2H 5G5  
Telephone: (519) 571-9833 Fax:

#### Location of Proposal:

705 Kingston Road, Pickering

Municipality: Lot(s): Concession:

Durham Region File No. (if available):

Name of Property Owner (if available):

**Date Request Received:** September 28, 2024

Received By: Anthony Caruso

**Date Forecast Sent:** October 4, 2024

Name of Road Segment	Forecasted AADT*	No. of Lanes	% of Trucks	Heavy : Medium Truck Ratio		Speed (km/h)
Kingston Road (Whites to Fairport)	35,000	4	8	30	70	60
Whites Road (Kingston to Sheppard)	35,000	6	10	70	30	60

\* Average Annual Daily Traffic. Forecast based on ultimate development according to the Durham Regional Official Plan.

Thanks

Callum



**Callum Heggart**  
**Dillon Consulting Limited**  
Suite 200 - 51 Breithaupt Street  
Kitchener, Ontario, N2H 5G5

C - 519.577.7832  
T - 519.571.9833 ext. 3153  
[CHeggart@dillon.ca](mailto:CHeggart@dillon.ca)  
[www.dillon.ca](http://www.dillon.ca)

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## The Regional Municipality of Durham

Planning and Economic  
Development Department

Planning Division

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[www.durham.ca](http://www.durham.ca)

**Brian Bridgeman, MCIP, RPP, PLE**  
Commissioner of Planning and  
Economic Development

### ROAD SEGMENT TRAFFIC FORECASTS FOR NOISE ANALYSES

This information is to be used as the basis for assessing the potential impacts of noise, generated by traffic on Provincial Highways and arterial roads, on proposed land uses that are sensitive (e.g., residential subdivisions). Arterial roads include existing and future Type A, B and C, as designated in the Durham Regional Official Plan.

Noise assessment reports recommend specific measures to be integrated into the design of sensitive developments to reduce road noise impacts to acceptable levels.

#### Provided For:

Name / Name of Firm: Callie Airdrie, Dillion Consulting Ltd  
Address: 51 Breithaupt Street, Suite 200, Kitchener, ON N2H 5G5  
Telephone: (519) 571-9833 Fax:

#### Location of Proposal:

705 Kingston Road, Pickering

Municipality: Lot(s): Concession:

Durham Region File No. (if available):

Name of Property Owner (if available):

**Date Request Received:** September 28, 2024

Received By: Anthony Caruso

**Date Forecast Sent:** October 4, 2024

Name of Road Segment	Forecasted AADT*	No. of Lanes	% of Trucks	Heavy : Medium Truck Ratio		Speed (km/h)
Kingston Road (Whites to Fairport)	35,000	4	8	30	70	60
Whites Road (Kingston to Sheppard)	35,000	6	10	70	30	60

\* Average Annual Daily Traffic. Forecast based on ultimate development according to the Durham Regional Official Plan.





Airdrie, Callie &lt;cairdrie@dillon.ca&gt;

---

## Road Traffic Information Request - 401

---

**Patel, Sohil (MTO)** <Sohil.Patel@ontario.ca>

Tue, Oct 1, 2024 at 9:34 AM

To: "Airdrie, Callie" &lt;cairdrie@dillon.ca&gt;

Cc: "Schmid, Kelly (MTO)" &lt;Kelly.Schmid@ontario.ca&gt;, "Bever, Cameron (MTO)" &lt;Cameron.Bever@ontario.ca&gt;, "Sedkowski, Martin (MTO)" &lt;Martin.Sedkowski@ontario.ca&gt;

Hello Callie,

Please see attached hourly volume available for closet location at Highway 401 and study site. Unfortunately, MTO doesn't have vehicle classification counts.

In the year of 2021, The AADT was 267,400 and %Truck was 10%.

Thank you,

**Sohil Patel, Traffic Analyst**

Highway Operations Management Branch

Operational Traffic Engineering Section

Ministry of Transportation,

301 St Paul St, St. Catharines, ON L2R 7R4

---

**From:** Airdrie, Callie <cairdrie@dillon.ca>

**Sent:** Monday, September 30, 2024 11:26 AM

**To:** Christopher.Bee@ontario.ca

**Cc:** Patel, Sohil (MTO) <Sohil.Patel@ontario.ca>; Schmid, Kelly (MTO) <Kelly.Schmid@ontario.ca>

**Subject:** Re: Road Traffic Information Request - 401

**CAUTION -- EXTERNAL E-MAIL - Do not click links or open attachments unless you recognize the sender.**

Good morning,

I would like to follow up on this request to ask additionally for the Summer Average Daily Traffic for the property noted above.

Thanks,

Callie

On Fri, Sep 27, 2024 at 8:49 AM Airdrie, Callie <[cairdrie@dillon.ca](mailto:cairdrie@dillon.ca)> wrote:

Hi Christopher,

On behalf of the Resident, Dillon Consulting Ltd. is completing a Noise Feasibility Study for a proposed development located at [705 Kingston road](#) in Pickering, Ontario.

To support the Noise Feasibility Study I would like to request traffic information for the 401. Please let me know if the following information can be made available:

- Expected annual growth rate
- Medium and heavy truck percentage
- AADT

Thanks,

Callie

--

**Callie Airdrie**  
**Dillon Consulting Limited**  
51 Breithaupt Street Suite 200  
Kitchener, Ontario, N2H 5G5  
T - 519.571.9833 ext. 3159  
[cairdrie@dillon.ca](mailto:cairdrie@dillon.ca)  
[www.dillon.ca](http://www.dillon.ca)

**Callie Airdrie**  
**Dillon Consulting Limited**  
51 Breithaupt Street Suite 200  
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[www.dillon.ca](http://www.dillon.ca)

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---

**3 attachments**



**Hwy 401-Whites Rd-EB-Express-Seven Day Report - Hourly (401DE0560DEE,47610) 2023-07-04.pdf**  
11K



**Hwy 401-Whites Rd- WB-collector-Seven Day Report - Hourly (401DE0510DWC,47610) 2024-07-16.pdf**  
11K



**Hwy 401-Whites Rd- WB-express-Seven Day Report - Hourly (401DE0510DWE,47610) 2024-07-16.pdf**  
11K

# SEVEN DAY HOURLY REPORT

**Station 1:** 401DE0560DEE  
**HIGHWAY:** 401 **STREAM:** EXPRESS **DIRECTION:** EAST BOUND  
**LHRS / OFFSET:** 47610 / 2.25 **LOCATION:** (43.819, -79.111) **CONFIDENCE LEVEL:** 95%  
**DESCRIPTION** E. OF WHITES

HOUR-ENDING	TUE	WED	THU	FRI	SAT	SUN	MON
	04-Jul.-23	05-Jul.-23	06-Jul.-23	07-Jul.-23	08-Jul.-23	09-Jul.-23	10-Jul.-23
	NITS	NITS	NITS	NITS	NITS	NITS	NITS
01:00	1521	1575	1574	1759	2128	2242	1536
02:00	942	888	954	1063	1413	1459	1039
03:00	704	691	700	752	995	1137	683
04:00	606	657	N/A	728	864	824	N/A
05:00	728	775	775	838	748	N/A	764
06:00	1657	1407	1595	1566	1088	759	1563
07:00	2750	2721	2600	2743	1776	1206	2830
08:00	3054	3052	3095	3301	2674	1993	3098
09:00	2887	2894	2911	3120	3348	2474	2845
10:00	2924	2647	2853	3399	3774	3222	2983
11:00	3084	3367	3062	3552	3742	3520	3278
12:00	2963	3164	3259	3882	3798	4050	3339
13:00	3192	3380	3440	3684	3845	4187	3173
14:00	3597	3617	3643	3618	3629	4127	3706
15:00	3577	3827	3578	3463	3838	3845	3746
16:00	3611	3455	3506	3117	3574	3697	3253
17:00	3898	3626	3747	3890	3490	3741	3152
18:00	3694	3712	3584	3847	3414	3584	3111
19:00	3817	3574	3867	3878	3423	3476	3502
20:00	3443	3579	3754	3669	3251	3346	3139
21:00	2995	3293	3482	3397	3016	3281	3273
22:00	2641	2823	2906	3142	2989	3072	2654
23:00	1914	2427	2541	2821	3050	2510	2119
23:59	1889	2138	1991	2245	2675	1947	1750

24 Hr Total	62,088	63,289	63,417	67,474	66,542	63,699	60,536
A.M. Total	23,820	23,838	23,378	26,703	26,348	22,886	23,958
P.M. Total	38,268	39,451	40,039	40,771	40,194	40,813	36,578
Noon-Noon		62,106	62,829	66,742	67,119	63,080	64,771
Highest Hour Starting	16:00	14:00	18:00	16:00	12:00	12:00	14:00
Highest Hour Volume	3,898	3,827	3,867	3,890	3,845	4,187	3,746
ADT =	63,864	AWD =		64,112			

ADT (Average Daily Traffic)-The average daily volume of the days being

LHRS (Linear Highway Reference

AWD (Average Weekday Traffic) - The average weekday traffic based on data taken from Monday @noon to Friday @noon.

# SEVEN DAY HOURLY REPORT

<b>Station 1:</b>	401DE0510DWC				
HIGHWAY:	401	STREAM:	COLLECTORS	DIRECTION:	WEST BOUND
LHRS / OFFSET:	47610 / 2.5	LOCATION:	(43.817, -79.114)	CONFIDENCE LEVEL:	95%
DESCRIPTION	WHITES				

HOUR-ENDING	TUE	WED	THU	FRI	SAT	SUN	MON
	16-Jul.-24	17-Jul.-24	18-Jul.-24	19-Jul.-24	20-Jul.-24	21-Jul.-24	22-Jul.-24
	NITS	NITS	NITS	NITS	NITS	NITS	NITS
01:00	N/A	893	896	1172	1499	1685	N/A
02:00	N/A	N/A	N/A	N/A	1019	1115	N/A
03:00	N/A	N/A	N/A	N/A	N/A	856	N/A
04:00	N/A	N/A	N/A	N/A	N/A	N/A	N/A
05:00	1143	1150	1034	1189	N/A	N/A	1003
06:00	3718	3685	3418	3347	1192	N/A	3273
07:00	4922	5002	4938	4154	1570	1326	4485
08:00	4866	4949	4785	3885	1820	1332	4289
09:00	4689	4692	4654	3985	2593	1799	4242
10:00	3597	3948	3937	3636	3335	2410	3745
11:00	3123	3427	3536	3487	3769	3244	3219
12:00	2673	3353	3482	3439	3929	3512	3133
13:00	2693	3314	3414	3525	3958	3647	3219
14:00	2850	3343	3487	3543	3981	N/A	3214
15:00	3231	3544	3671	3653	3995	3773	3458
16:00	3473	3713	3955	3621	3781	3792	3482
17:00	3732	3838	4118	3950	3774	3891	3664
18:00	3636	3779	4039	4064	3886	4027	3788
19:00	3254	3582	3665	3759	3917	4008	3408
20:00	2852	3059	3282	3636	3556	3562	3091
21:00	2539	2694	2908	2972	3020	3340	2804
22:00	2589	2743	2918	2996	2927	3089	2444
23:00	2157	2367	2366	2719	2833	2780	1828
23:59	1346	1549	1681	2140	2406	1448	1208

24 Hr Total	63,083	68,624	70,184	68,872	62,760	54,636	62,997
A.M. Total	28,731	31,099	30,680	28,294	20,726	17,279	27,389
P.M. Total	34,352	37,525	39,504	40,578	42,034	37,357	35,608
Noon-Noon		65,451	68,205	67,798	61,304	59,313	64,746
Highest Hour Starting	06:00	06:00	06:00	06:00	14:00	17:00	06:00
Highest Hour Volume	4,922	5,002	4,938	4,154	3,995	4,027	4,485
ADT =	64,451	AWD =		66,550			

ADT (Average Daily Traffic)-The average daily volume of the days being

LHRS (Linear Highway Reference

AWD (Average Weekday Traffic) - The average weekday traffic based on data taken from Monday @noon to Friday @noon.

# SEVEN DAY HOURLY REPORT

Station 1:	401DE0510DWE				
HIGHWAY:	401	STREAM:	EXPRESS	DIRECTION:	WEST BOUND
LHRS / OFFSET:	47610 / 2.5	LOCATION:	(43.817, -79.114)	CONFIDENCE LEVEL:	95%
DESCRIPTION	WHITES				

HOUR-ENDING	TUE	WED	THU	FRI	SAT	SUN	MON
	16-Jul.-24	17-Jul.-24	18-Jul.-24	19-Jul.-24	20-Jul.-24	21-Jul.-24	22-Jul.-24
	NITS	NITS	NITS	NITS	NITS	NITS	NITS
01:00	663	714	816	707	1059	1212	1088
02:00	N/A	492	599	N/A	699	791	772
03:00	477	476	470	N/A	N/A	N/A	583
04:00	524	527	632	542	539	N/A	588
05:00	1133	1135	1338	899	582	N/A	1298
06:00	3428	3491	3716	3064	996	N/A	3678
07:00	3767	3829	3683	3579	1669	992	4093
08:00	3686	3622	3529	3688	2237	1107	4044
09:00	3383	3281	3161	3319	2897	1655	3490
10:00	2779	3167	3165	3141	3457	2889	3261
11:00	2337	3143	3074	3205	3688	3726	3178
12:00	2223	3035	2952	3222	3594	4058	3001
13:00	2095	3074	2924	3005	3627	3838	3018
14:00	2644	2996	2817	3132	3643	N/A	3058
15:00	2629	2830	2653	3052	3555	3778	2906
16:00	2773	2958	2732	3023	3515	3856	2930
17:00	2660	2748	2676	3065	3463	3946	2896
18:00	2718	2968	2876	3096	3650	4050	3060
19:00	2660	2863	2816	3093	3628	3979	3099
20:00	2512	2739	2894	3310	3560	3803	3082
21:00	2229	2444	2633	2993	3359	3743	2664
22:00	1754	1935	2017	2812	3315	3618	2232
23:00	1378	1391	1494	2362	2683	3143	1877
23:59	946	1025	1065	1320	1736	1625	1237

24 Hr Total	51,398	56,883	56,732	59,629	61,151	55,809	61,133
A.M. Total	24,400	26,912	27,135	25,366	21,417	16,430	29,074
P.M. Total	26,998	29,971	29,597	34,263	39,734	39,379	32,059
Noon-Noon		53,910	57,106	54,963	55,680	56,164	68,453
Highest Hour Starting	06:00	06:00	05:00	07:00	10:00	11:00	06:00
Highest Hour Volume	3,767	3,829	3,716	3,688	3,688	4,058	4,093
ADT =	57,534	AWD =		58,608			

ADT (Average Daily Traffic)-The average daily volume of the days being

LHRS (Linear Highway Reference

AWD (Average Weekday Traffic) - The average weekday traffic based on data taken from Monday @noon to Friday @noon.



Airdrie, Callie &lt;cairdrie@dillon.ca&gt;

---

**KNG-313.04- Liverpool Road, Pickering ON Rail Volume Information Request**

---

Sarangan Srikanth <Sarangan.Srikanth@cn.ca>  
To: "Airdrie, Callie" <cairdrie@dillon.ca>

Tue, Oct 15, 2024 at 9:26 AM

Hi Callie,

The attached document is regarding your request for the Train Traffic Data for the following location: KNG-313.04- Liverpool Road, Pickering ON; this data does not reflect GO Metrolinx Traffic.

If you have any additional questions, please feel free to reach out to me.

Thank you,

**Sarangan Srikanth**

Officer Public Works | Engineering-GLD- Eastern Canada  
T: 905-669-3000 | C: 437-329-4963

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---

**From:** Airdrie, Callie <cairdrie@dillon.ca>  
**Sent:** Friday, September 27, 2024 9:08 AM  
**To:** GLD-Permits <permits.gld@cn.ca>  
**Subject:** Rail Volume Information Request

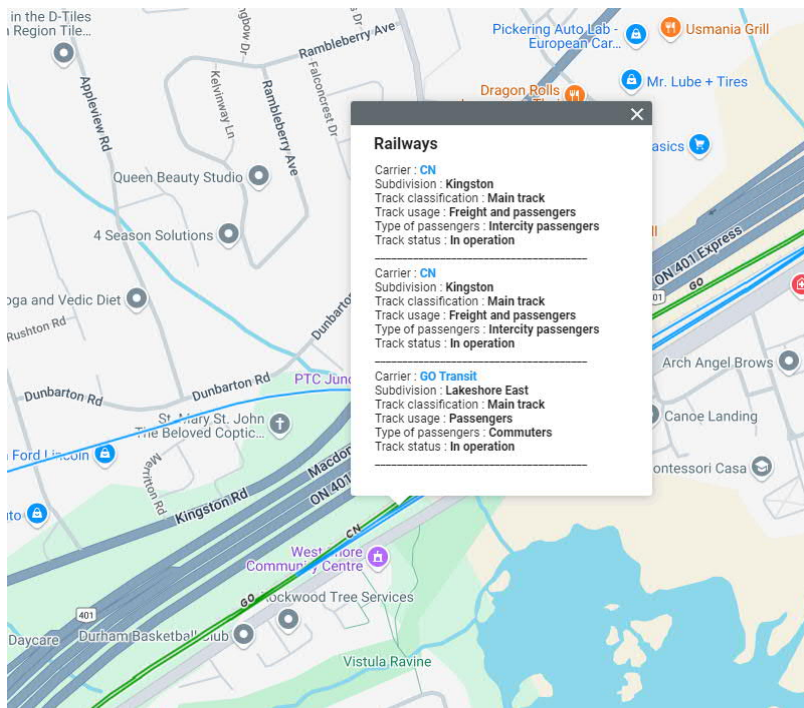
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Good morning,

I have been retained to complete a noise feasibility study for a proposed residential development in the city of Pickering. As the proposed development is in proximity to a CN rail line, I would like to request rail data for the purpose of noise modelling. The rail line I am interested in is pictured below (Kingston Subdivision).

Can you please provide rail traffic volumes and all relevant information to complete the noise study including speed, whistle activity, and track conditions?



Thanks,

Callie

--



**Callie Airdrie**  
**Dillon Consulting Limited**  
51 Breithaupt Street Suite 200  
Kitchener, Ontario, N2H 5G5  
T - 519.571.9833 ext. 3159  
cairdrie@dillon.ca  
www.dillon.ca

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**Train Count Response - KNG - 313.04 - Liverpool Rd, Pickering ON.pdf**  
352K





# Train Count Data

## TRANSMITTAL

To: Dillon Consulting  
Destinataire : Limited  
51 Breithaupt Street  
Suite 200  
Kitchener, Ontario,  
N2H 5G5

Project : KNG - 313.04 - Liverpool Rd, Pickering ON

Att'n: Callie Airdrie

Routing: cairdrie@dillon.ca

From: Sarangan Srikanth  
Expéditeur :

Date: 2024/10/15

Cc: Adjacent Development  
CN via e-mail

☐ Urgent ☐ For Your Use ☐ For Review ☒ For Your Information ☐ Confidential

**Re: Train Traffic Data – CN Kingston Subdivision near Liverpool Road  
in Pickering ON**

Please find attached the requested Train Traffic Data; this data does not reflect GO Metrolinx Traffic. The application fee in the amount of **\$500.00 +HST** will be invoiced.

Should you have any questions, please do not hesitate to contact the undersigned at [permits.gld@cn.ca](mailto:permits.gld@cn.ca).

Sincerely,

*Sarangan Srikanth*

Sarangan Srikanth  
Officer Public Works  
[Permits.gld@cn.ca](mailto:Permits.gld@cn.ca)

**Date:** 2024/10/15

**Project Number:** KNG - 313.04 – Liverpool Road, Pickering ON

Dear Callie:

**Re: Train Traffic Data – CN Kingston Subdivision near Liverpool Road in Pickering ON**

The following is provided in response to Callie's 2023/02/17 request for information regarding rail traffic in the vicinity of Liverpool Road in Pickering, ON at approximately Mile 313.04 on CN's Kingston Subdivision.

Typical daily traffic volumes are recorded below. However, traffic volumes may fluctuate due to overall economic conditions, varying traffic demands, weather conditions, track maintenance programs, statutory holidays and traffic detours that when required may be heavy although temporary. For the purpose of noise and vibration reports, train volumes must be escalated by 2.5% per annum for a 10-year period.

Typical daily traffic volumes at this site location are as follows:

**\*Maximum train speed is given in Miles per Hour**

	0700-2300			
Type of Train	Volumes	Max.Consist	Max. Speed	Max. Power
Freight	12	140	65	4
Way Freight	0	25	65	4
Passenger	34	10	100	2

	2300-0700			
Type of Train	Volumes	Max.Consist	Max. Speed	Max. Power
Freight	5	140	65	4
Way Freight	4	25	65	4
Passenger	1	10	100	2

The volumes recorded reflect westbound and eastbound freight and passenger operations on CN's Kingston Subdivision.

Except where anti-whistling bylaws are in effect, engine-warning whistles and bells are normally sounded at all at-grade crossings. There are no at-grade crossing in the immediate vicinity of the study area. Please note that engine warning whistles may be sounded in cases of emergency, as a safety and or warning precaution at station locations and pedestrian crossings and occasionally for operating requirements.

With respect to equipment restrictions, the gross weight of the heaviest permissible car is 286,000 lbs.

The triple (3) mainline track is considered to be continuously welded rail throughout the study area. The presence of 4 switches located at Mile 313.02, 313.04, 313.12, and 313.13 may exacerbate the noise and vibration caused by train movements.

The Canadian National Railway continues to be strongly opposed to locating developments near railway facilities and rights-of-way due to potential safety and environmental conflicts. Development adjacent to the Railway Right-of-Way is not appropriate without sound impact mitigation measures to reduce the incompatibility. For confirmation of the applicable rail noise, vibration and safety standards, Adjacent Development, Canadian National Railway Properties at [Proximity@cn.ca](mailto:Proximity@cn.ca) should be contacted directly.

I trust the above information will satisfy your current request.

Sincerely,

*Sarangan Srikanth*

Sarangan Srikanth  
Officer Public Works  
[Permits.gld@cn.ca](mailto:Permits.gld@cn.ca)

Rail Information Request

Rail Data Requests <RailDataRequests@metrolinx.com>  
To: "Heggart, Callum" <CHeggart@dillon.ca>

Fri, Nov 29, 2024 at 4:07 PM

Hi Callum,

Further to your request dated November 29, 2024, the subject lands ([1095 Kingston Road, Pickering](#)) are located within 300 metres of the Metrolinx Kingston Subdivision (which carries Lakeshore East GO rail service).

It's anticipated that GO rail service on this Subdivision will be comprised of diesel and electric trains. The GO rail fleet combination on this Subdivision will consist of up to 1 locomotive and 5 passenger cars. The typical GO rail weekday train volume forecast near the subject lands, including both revenue and equipment trips is in the order of 324 trains. The planned detailed trip breakdown is listed below:

	1 Diesel Locomotive	1 Electric Locomotive		1 Diesel Locomotive	1 Electric Locomotive
Day (0700-2300)	64	213	Night (2300-0700)	10	37

The current track design speed near the subject lands is 100 mph (161 km/h).

There are no *anti-whistling by-laws* in affect near the subject lands.

With respect to future electrified rail service, Metrolinx is committed to finding the most sustainable solution for electrifying the GO rail network and we are currently working towards the next phase.

Options have been studied as part of the Transit Project Assessment Process (TPAP) for the GO Expansion program, currently in the Development Phase. ONxpress will be responsible for selecting and delivering the right trains and infrastructure to unlock the benefits of GO Expansion. Construction to support GO Expansion is currently underway.

However, we can advise that train noise is dominated by the powertrain at lower speeds and by the wheel- track interaction at higher speeds. Hence, the noise level and spectrum of electric trains is expected to be very similar at higher speeds, if not identical, to those of equivalent diesel trains.

Given the above considerations, it would be prudent at this time, for the purposes of acoustical analyses for development in proximity to Metrolinx corridors, to assume that the acoustical characteristics of electrified and diesel trains are equivalent. In light of the aforementioned information, acoustical models should employ diesel train parameters as the basis for analyses. We anticipate that additional information regarding specific operational parameters for electrified trains will become available in the future once the proponent team is selected.

Operational information is subject to change and may be influenced by, among other factors, service planning priorities, operational considerations, funding availability and passenger demand.

It should be noted that this information only pertains to Metrolinx rail service. It would be prudent to contact other rail operators in the area directly for rail traffic information pertaining to non-Metrolinx rail service.

I trust this information is useful. Should you have any questions or concerns, please do not hesitate to contact me.

Best Regards,

**Jenna Auger (She/Her)**

Third Party Projects Review (TPPR)

Development & Real Estate Management

T: (416)-881-0579

[10 Bay Street | Toronto | Ontario | M5J 2N8](#)



---

**From:** Heggart, Callum <[cheggart@dillon.ca](mailto:cheggart@dillon.ca)>  
**Sent:** Friday, November 29, 2024 3:48 PM  
**To:** Rail Data Requests <[RailDataRequests@metrolinx.com](mailto:RailDataRequests@metrolinx.com)>  
**Subject:** Rail Information Request

You don't often get email from [cheggart@dillon.ca](mailto:cheggart@dillon.ca). [Learn why this is important](#)

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Hi,

I have been retained to complete a noise feasibility study for a proposed residential development located at [1095 Kingston Road](#) in Pickering, Ontario. As the proposed development is in proximity to the Go Transit Lakeshore East Subdivision, I would like to request rail data for the purpose of noise modelling.

Can you please provide rail traffic volumes and all relevant information to complete the noise study including speed, whistle activity, and track conditions?

Thanks

Callum

**Callum Heggart**  
**Dillon Consulting Limited**  
Suite 200 - 51 Breithaupt Street  
Kitchener, Ontario, N2H 5G5  
  
C - 519,577,7832  
T - 519,571.9833 ext. 3153  
[CHeggart@dillon.ca](mailto:CHeggart@dillon.ca)  
[www.dillon.ca](http://www.dillon.ca)

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## Appendix D

### Stamson Outputs

Filename: POR2B\_AD.te Time Period: 1 hours  
Description: POR2B Ambient Daytime

Road data, segment # 1: 401EE  
-----

Car traffic volume : 1085 veh/TimePeriod  
Medium truck volume : 30 veh/TimePeriod  
Heavy truck volume : 90 veh/TimePeriod  
Posted speed limit : 100 km/h  
Road gradient : 0 %  
Road pavement : 1 (Typical asphalt or concrete)

Data for Segment # 1: 401EE  
-----

Angle1 Angle2 : 0.00 deg 30.00 deg  
Wood depth : 0 (No woods.)  
No of house rows : 0  
Surface : 1 (Absorptive ground surface) Receiver source distance : 140.00 m  
Receiver height : 17.50 m  
Topography : 1 (Flat/gentle slope; no barrier) Reference angle : 0.00

Road data, segment # 2: 401WC  
-----

Car traffic volume : 1193 veh/TimePeriod  
Medium truck volume : 33 veh/TimePeriod  
Heavy truck volume : 99 veh/TimePeriod  
Posted speed limit : 100 km/h  
Road gradient : 0 %  
Road pavement : 1 (Typical asphalt or concrete)

Data for Segment # 2: 401WC  
-----

Angle1 Angle2 : 0.00 deg 30.00 deg  
Wood depth : 0 (No woods.)  
No of house rows : 0  
Surface : 1 (Absorptive ground surface) Receiver source distance : 100.00 m  
Receiver height : 17.50 m  
Topography : 1 (Flat/gentle slope; no barrier) Reference angle : 0.00

Road data, segment # 3: 401WE  
-----

Car traffic volume : 893 veh/TimePeriod  
Medium truck volume : 25 veh/TimePeriod Heavy truck volume : 74 veh/  
TimePeriod  
Posted speed limit : 100 km/h  
Road gradient : 0 %  
Road pavement : 1 (Typical asphalt or concrete)



Data for Segment # 3: 401WE

-----

Angle1 Angle2 : 0.00 deg 30.00 deg

Wood depth : 0 (No woods.)

No of house rows : 0

Surface : 1 (Absorptive ground surface) Receiver source distance : 120.00 m

Receiver height : 17.50 m

Topography : 1 (Flat/gentle slope; no barrier) Reference angle : 0.00

Results segment # 1: 401EE

-----

Source height = 1.65 m

ROAD (0.00 + 56.93 + 0.00) = 56.93 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq	-----
										0 30	-----
0.18	76.15	0.00	-11.40	-7.82	0.00	0.00	0.00	56.93	-----		-----

Segment Leq : 56.93 dBA

Results segment # 2: 401WC

-----

Source height = 1.65 m

ROAD (0.00 + 59.06 + 0.00) = 59.06 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq	-----
										0 30	-----
0.18	76.57	0.00	-9.68	-7.82	0.00	0.00	0.00	59.06	-----		-----

Segment Leq : 59.06 dBA

Results segment # 3: 401WE

-----

Source height = 1.65 m

ROAD (0.00 + 56.88 + 0.00) = 56.88 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq	-----
										0 30	-----
0.18	75.31	0.00	-10.62	-7.82	0.00	0.00	0.00	56.88	-----		-----

Segment Leq : 56.88 dBA

Total Leq All Segments: 62.52 dBA

TOTAL Leq FROM ALL SOURCES: 62.52

Filename: por21a\_e.te Time Period: 1 hours  
Description: POR2B Ambient Evening

Road data, segment # 1: 401EE  
-----

Car traffic volume : 2377 veh/TimePeriod  
Medium truck volume : 66 veh/TimePeriod  
Heavy truck volume : 198 veh/TimePeriod  
Posted speed limit : 100 km/h  
Road gradient : 0 %  
Road pavement : 1 (Typical asphalt or concrete)

Data for Segment # 1: 401EE  
-----

Angle1 Angle2 : 0.00 deg 30.00 deg  
Wood depth : 0 (No woods.)  
No of house rows : 0  
Surface : 1 (Absorptive ground surface) Receiver source distance : 140.00 m  
Receiver height : 17.50 m  
Topography : 1 (Flat/gentle slope; no barrier) Reference angle : 0.00

Road data, segment # 2: 401WC  
-----

Car traffic volume : 2200 veh/TimePeriod  
Medium truck volume : 61 veh/TimePeriod  
Heavy truck volume : 183 veh/TimePeriod  
Posted speed limit : 100 km/h  
Road gradient : 0 %  
Road pavement : 1 (Typical asphalt or concrete)

Data for Segment # 2: 401WC  
-----

Angle1 Angle2 : 0.00 deg 30.00 deg  
Wood depth : 0 (No woods.)  
No of house rows : 0  
Surface : 1 (Absorptive ground surface) Receiver source distance : 120.00 m  
Receiver height : 17.50 m  
Topography : 1 (Flat/gentle slope; no barrier) Reference angle : 0.00

Road data, segment # 3: 401WE  
-----

Car traffic volume : 1579 veh/TimePeriod  
Medium truck volume : 44 veh/TimePeriod Heavy truck volume : 132 veh/  
TimePeriod  
Posted speed limit : 100 km/h  
Road gradient : 0 %  
Road pavement : 1 (Typical asphalt or concrete)

Data for Segment # 3: 401WE

-----

Angle1 Angle2 : 0.00 deg 30.00 deg

Wood depth : 0 (No woods.)

No of house rows : 0

Surface : 1 (Absorptive ground surface) Receiver source distance : 100.00 m

Receiver height : 17.50 m

Topography : 1 (Flat/gentle slope; no barrier) Reference angle : 0.00

Results segment # 1: 401EE

-----

Source height = 1.65 m

ROAD (0.00 + 60.35 + 0.00) = 60.35 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq	-----
										0 30	-----
0.18	79.57	0.00	-11.40	-7.82	0.00	0.00	0.00	60.35	-----		

Segment Leq : 60.35 dBA

Results segment # 2: 401WC

-----

Source height = 1.65 m

ROAD (0.00 + 60.80 + 0.00) = 60.80 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq	-----
										0 30	-----
0.18	79.23	0.00	-10.61	-7.82	0.00	0.00	0.00	60.80	-----		

Segment Leq : 60.80 dBA

Results segment # 3: 401WE

-----

Source height = 1.66 m

ROAD (0.00 + 60.30 + 0.00) = 60.30 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq	-----
										0 30	-----
0.18	77.81	0.00	-9.68	-7.82	0.00	0.00	0.00	60.30	-----		

Segment Leq : 60.30 dBA

Total Leq All Segments: 65.26 dBA

TOTAL Leq FROM ALL SOURCES: 65.26

Filename: por21a\_n.te Time Period: 1 hours  
Description: POR2B Ambient Nighttime

Road data, segment # 1: 401EE

-----  
Car traffic volume : 545 veh/TimePeriod  
Medium truck volume : 15 veh/TimePeriod  
Heavy truck volume : 45 veh/TimePeriod  
Posted speed limit : 100 km/h  
Road gradient : 0 %  
Road pavement : 1 (Typical asphalt or concrete)

Data for Segment # 1: 401EE

-----  
Angle1 Angle2 : 0.00 deg 30.00 deg  
Wood depth : 0 (No woods.)  
No of house rows : 0  
Surface : 1 (Absorptive ground surface) Receiver source distance : 140.00 m  
Receiver height : 17.50 m  
Topography : 1 (Flat/gentle slope; no barrier) Reference angle : 0.00

Road data, segment # 2: 401WC

-----  
Car traffic volume : 770 veh/TimePeriod  
Medium truck volume : 21 veh/TimePeriod  
Heavy truck volume : 64 veh/TimePeriod  
Posted speed limit : 100 km/h  
Road gradient : 0 %  
Road pavement : 1 (Typical asphalt or concrete)

Data for Segment # 2: 401WC

-----  
Angle1 Angle2 : 0.00 deg 30.00 deg  
Wood depth : 0 (No woods.)  
No of house rows : 0  
Surface : 1 (Absorptive ground surface) Receiver source distance : 100.00 m  
Receiver height : 17.50 m  
Topography : 1 (Flat/gentle slope; no barrier) Reference angle : 0.00

Road data, segment # 3: 401WE

-----  
Car traffic volume : 423 veh/TimePeriod  
Medium truck volume : 12 veh/TimePeriod Heavy truck volume : 35 veh/  
TimePeriod  
Posted speed limit : 100 km/h  
Road gradient : 0 %  
Road pavement : 1 (Typical asphalt or concrete)



Data for Segment # 3: 401WE

-----

Angle1 Angle2 : 0.00 deg 30.00 deg

Wood depth : 0 (No woods.)

No of house rows : 0

Surface : 1 (Absorptive ground surface) Receiver source distance : 120.00 m

Receiver height : 17.50 m

Topography : 1 (Flat/gentle slope; no barrier) Reference angle : 0.00

Results segment # 1: 401EE

-----

Source height = 1.65 m

ROAD (0.00 + 53.93 + 0.00) = 53.93 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq	-----
											0 30
0.18	73.15	0.00	-11.40	-7.82	0.00	0.00	0.00	53.93			-----

Segment Leq : 53.93 dBA

Results segment # 2: 401WC

-----

Source height = 1.65 m

ROAD (0.00 + 57.16 + 0.00) = 57.16 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq	-----
											0 30
0.18	74.66	0.00	-9.68	-7.82	0.00	0.00	0.00	57.16			-----

Segment Leq : 57.16 dBA

Results segment # 3: 401WE

-----

Source height = 1.65 m

ROAD (0.00 + 53.63 + 0.00) = 53.63 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq	-----
											0 30
0.18	72.06	0.00	-10.62	-7.82	0.00	0.00	0.00	53.63			-----

Segment Leq : 53.63 dBA

Total Leq All Segments: 59.99 dBA

TOTAL Leq FROM ALL SOURCES: 59.99

Filename: 1095comp.te Time Period: Day/Night 16/8 hours Description:  
Comparison to TNM. Tower 1 6th floor south facade

Road data, segment # 1: 401 WB CL (day/night) -----  
----- Car traffic volume : 94594/3220 veh/TimePeriod Medium truck  
volume : 2628/192 veh/TimePeriod Heavy truck volume : 7883/84 veh/TimePeriod  
Posted speed limit : 100 km/h Road gradient : 0 % Road pavement : 1 (Typical  
asphalt or concrete)

Data for Segment # 1: 401 WB CL (day/night) -----  
----- Angle1 Angle2 : -80.00 deg 90.00 deg Wood depth : 0 (No woods.) No  
of house rows : 0 / 0 Surface : 1 (Absorptive ground surface) Receiver  
source distance : 60.00 / 60.00 m  
Receiver height : 20.00 / 4.50 m Topography : 1 (Flat/gentle slope; no  
barrier) Reference angle : 0.00

Road data, segment # 2: 401 WB EX (day/night) -----  
----- Car traffic volume : 72058/3150 veh/TimePeriod Medium truck  
volume : 2002/105 veh/TimePeriod Heavy truck volume : 6005/245 veh/  
TimePeriod Posted speed limit : 100 km/h Road gradient : 0 % Road pavement :  
1 (Typical asphalt or concrete)

Data for Segment # 2: 401 WB EX (day/night) -----  
----- Angle1 Angle2 : -80.00 deg 90.00 deg Wood depth : 0 (No woods.) No  
of house rows : 0 / 0 Surface : 1 (Absorptive ground surface) Receiver  
source distance : 80.00 / 80.00 m Receiver height : 20.00 / 4.50 m Topography  
: 1 (Flat/gentle slope; no barrier)  
Reference angle : 0.00

Road data, segment # 3: 401 EB EX (day/night) -----  
----- Car traffic volume : 89536/18922 veh/TimePeriod Medium truck  
volume : 2487/525 veh/TimePeriod Heavy truck volume : 7461/1576 veh/  
TimePeriod Posted speed limit : 100 km/h Road gradient : 0 % Road pavement :  
1 (Typical asphalt or concrete)

Data for Segment # 3: 401 EB EX (day/night) -----  
----- Angle1 Angle2 : -80.00 deg 90.00 deg Wood depth : 0 (No woods.) No  
of house rows : 0 / 0 Surface : 1 (Absorptive ground surface) Receiver  
source distance : 100.00 / 100.00 m Receiver height : 20.00 / 4.50 m  
Topography : 1 (Flat/gentle slope; no barrier) Reference angle : 0.00

Results segment # 1: 401 WB CL (day) -----

Source height = 1.65 m

ROAD (0.00 + 76.42 + 0.00) = 76.42 dBA Angle1 Angle2 Alpha RefLeq P.Adj D.Adj  
F.Adj W.Adj H.Adj B.Adj SubLeq -----  
-----  
-80 90 0.10 83.53 0.00 -6.62 -0.49 0.00 0.00 0.00 76.42 -----  
-----

Segment Leq : 76.42 dBA

Results segment # 2: 401 WB EX (day) -----

Source height = 1.65 m

ROAD (0.00 + 73.86 + 0.00) = 73.86 dBA Angle1 Angle2 Alpha RefLeq P.Adj D.Adj  
F.Adj W.Adj H.Adj B.Adj SubLeq -----  
-----  
-80 90 0.10 82.35 0.00 -8.00 -0.49 0.00 0.00 0.00 73.86 -----  
-----

Segment Leq : 73.86 dBA

Results segment # 3: 401 EB EX (day) -----

Source height = 1.65 m

ROAD (0.00 + 73.74 + 0.00) = 73.74 dBA Angle1 Angle2 Alpha RefLeq P.Adj D.Adj  
F.Adj W.Adj H.Adj B.Adj SubLeq -----  
-----  
-80 90 0.10 83.29 0.00 -9.07 -0.49 0.00 0.00 0.00 73.74 -----  
-----

Segment Leq : 73.74 dBA

Total Leq All Segments: 79.63 dBA

Results segment # 1: 401 WB CL (night) -----  
-

Source height = 1.25 m

ROAD (0.00 + 59.32 + 0.00) = 59.32 dBA Angle1 Angle2 Alpha RefLeq P.Adj D.Adj  
F.Adj W.Adj H.Adj B.Adj SubLeq -----  
-----  
-80 90 0.58 70.21 0.00 -9.50 -1.39 0.00 0.00 0.00 59.32 -----  
-----

Segment Leq : 59.32 dBA

Results segment # 2: 401 WB EX (night) -----  
-

Source height = 1.63 m

ROAD (0.00 + 58.90 + 0.00) = 58.90 dBA Angle1 Angle2 Alpha RefLeq P.Adj D.Adj  
F.Adj W.Adj H.Adj B.Adj SubLeq -----  
-----  
-80 90 0.57 71.66 0.00 -11.39 -1.37 0.00 0.00 0.00 58.90 -----  
-----

Segment Leq : 58.90 dBA

Results segment # 3: 401 EB EX (night) -----

-

Source height = 1.65 m

ROAD (0.00 + 65.28 + 0.00) = 65.28 dBA Angle1 Angle2 Alpha RefLeq P.Adj D.Adj  
F.Adj W.Adj H.Adj B.Adj SubLeq -----

-----  
-80 90 0.57 79.55 0.00 -12.90 -1.37 0.00 0.00 0.00 65.28 -----  
-----

Segment Leq : 65.28 dBA

Total Leq All Segments: 66.99 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 79.63  
(NIGHT): 66.99

## Appendix E

### BPN Analysis







Receptor	Source	Time of Day	Location	Sound Levels				Façade and Room Inputs								Height of Receptor (m)	Horizontal Distance to Source (m)	Source Inputs			Component 1 - Veneer					Component 2 - Glazing					Required Glazing (STC)			
				Façade Level (dBA)	Free Field Correction (dBA)	Indoor Requirement (dBA)	Required Reduction (dBA)	Exposed Façade Height (m)	Exposed Façade Length (m)	Room Depth (m)	Floor Area (m²)	Façade Area (m²)	Glazing as % of Façade Area (%)	Glazing as % of Floor Area (%)	Veneer as % of Floor Area (%)			Room Absorption	Incident Sound Angle (deg)	Angle Correction	Source Spectrum	Assumed Veneer (STC)	Building Component	Spectrum Correction	Room Correction	% Total Transmitted Energy (%)	Energy Correction	Building Component	Spectrum Correction	Room Correction		% Total Transmitted Energy (%)	Energy Correction	
Tower 1 L7 to L8 West	Roadway	Daytime	Living/Dining	74	3	45	32	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	24	20	50.19	2	D	54	D	7	-4	5%	51	C	4	-1	95%	0	35	Living / Dining Areas
	Locomotive	Daytime	Living/Dining	64	3	40	27	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	24	60	21.80	0	F	54	D	10	-4	5%	48	C	6	-1	95%	0	32	
	Wheel	Daytime	Living/Dining	68	3	40	31	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	24	60	21.80	0	B	54	D	2	-4	5%	56	C	1	-1	95%	0	31	
																																38		
	Roadway	Night-time	Living/Dining	69	3	45	27	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	24	20	50.19	2	D	54	D	7	-4	5%	51	C	4	-1	95%	0	31	
	Locomotive	Night-time	Living/Dining	63	3	40	26	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	24	60	21.80	0	F	54	D	10	-4	5%	48	C	6	-1	95%	0	31	
	Wheel	Night-time	Living/Dining	67	3	40	30	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	24	60	21.80	0	B	54	D	2	-4	5%	56	C	1	-1	95%	0	31	
	Roadway	Daytime	Sleeping Quarters	74	3	45	32	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	24	20	50.19	2	D	54	D	7	-2	5%	49	C	4	-2	95%	0	34	38
	Locomotive	Daytime	Sleeping Quarters	64	3	40	27	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	24	60	21.80	0	F	54	D	10	-2	5%	46	C	6	-2	95%	0	31	Sleeping Quarters
	Wheel	Daytime	Sleeping Quarters	68	3	40	31	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	24	60	21.80	0	B	54	D	2	-2	5%	54	C	1	-2	95%	0	30	
																																37		
	Roadway	Night-time	Sleeping Quarters	69	3	40	32	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	24	20	50.19	2	D	54	D	7	-2	5%	49	C	4	-2	95%	0	35	
Locomotive	Night-time	Sleeping Quarters	63	3	35	31	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	24	60	21.80	0	F	54	D	10	-2	5%	46	C	6	-2	95%	0	35		
Wheel	Night-time	Sleeping Quarters	67	3	35	35	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	24	60	21.80	0	B	54	D	2	-2	5%	54	C	1	-2	95%	0	34		
																															39	39		
Tower 1A L9 to L35 North	Roadway	Daytime	Living/Dining	70	3	45	28	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	45	D	7	-4	5%	42	C	4	-1	95%	0	31	Living / Dining Areas
	Locomotive	Daytime	Living/Dining	59	3	40	22	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	F	45	D	10	-4	5%	39	C	6	-1	95%	0	28	
	Wheel	Daytime	Living/Dining	63	3	40	26	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	B	45	D	2	-4	5%	47	C	1	-1	95%	0	27	
																																34		
	Roadway	Night-time	Living/Dining	66	3	45	24	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	45	D	7	-4	5%	42	C	4	-1	95%	0	27	
	Locomotive	Night-time	Living/Dining	57	3	40	20	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	F	45	D	10	-4	5%	39	C	6	-1	95%	0	26	
	Wheel	Night-time	Living/Dining	61	3	40	24	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	B	45	D	2	-4	5%	47	C	1	-1	95%	0	25	
	Roadway	Daytime	Sleeping Quarters	70	3	45	28	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	45	D	7	-2	5%	40	C	4	-2	95%	0	30	Sleeping Quarters
	Locomotive	Daytime	Sleeping Quarters	59	3	40	22	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	F	45	D	10	-2	5%	37	C	6	-2	95%	0	27	
	Wheel	Daytime	Sleeping Quarters	63	3	40	26	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	B	45	D	2	-2	5%	45	C	1	-2	95%	0	25	
																																33		
	Roadway	Night-time	Sleeping Quarters	66	3	40	29	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	45	D	7	-2	5%	40	C	4	-2	95%	0	31	
Locomotive	Night-time	Sleeping Quarters	57	3	35	25	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	F	45	D	10	-2	5%	37	C	6	-2	95%	0	29		
Wheel	Night-time	Sleeping Quarters	61	3	35	29	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	B	45	D	2	-2	5%	45	C	1	-2	95%	0	28		
																															34	34		
Tower 1A L9 to L35 East	Roadway	Daytime	Living/Dining	77	3	45	35	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	54	D	7	-4	5%	51	C	4	-1	95%	0	39	Living / Dining Areas
	Locomotive	Daytime	Living/Dining	66	3	40	29	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	F	54	D	10	-4	5%	48	C	6	-1	95%	0	35	
	Wheel	Daytime	Living/Dining	70	3	40	33	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	B	54	D	2	-4	5%	56	C	1	-1	95%	0	33	
																																41		
	Roadway	Night-time	Living/Dining	73	3	45	31	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	54	D	7	-4	5%	51	C	4	-1	95%	0	35	
	Locomotive	Night-time	Living/Dining	64	3	40	27	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	F	54	D	10	-4	5%	48	C	6	-1	95%	0	33	
	Wheel	Night-time	Living/Dining	68	3	40	31	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	B	54	D	2	-4	5%	56	C	1	-1	95%	0	32	
	Roadway	Daytime	Sleeping Quarters	77	3	45	35	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	54	D	7	-2	5%	49	C	4	-2	95%	0	37	Sleeping Quarters
	Locomotive	Daytime	Sleeping Quarters	66	3	40	29	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	F	54	D	10	-2	5%	46	C	6	-2	95%	0	33	
	Wheel	Daytime	Sleeping Quarters	70	3	40	33	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	B	54	D	2	-2	5%	54	C	1	-2	95%	0	32	
																																40		
	Roadway	Night-time	Sleeping Quarters	73	3	40	36	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	54	D	7	-2	5%	49	C	4	-2	95%	0	39	
Locomotive	Night-time	Sleeping Quarters	64	3	35	32	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	F	54	D	10	-2	5%	46	C	6	-2	95%	0	36		
Wheel	Night-time	Sleeping Quarters	68	3	35	36	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	B	54	D	2	-2	5%	54	C	1	-2	95%	0	35		
																															42	42		

Receptor	Source	Time of Day	Location	Sound Levels				Façade and Room Inputs								Height of Receptor (m)	Horizontal Distance to Source (m)	Source Inputs			Component 1 - Veneer				Component 2 - Glazing				Required Glazing (STC)					
				Façade Level (dBA)	Free Field Correction (dBA)	Indoor Requirement (dBA)	Required Reduction (dBA)	Exposed Façade Height (m)	Exposed Façade Length (m)	Room Depth (m)	Floor Area (m²)	Façade Area (m²)	Glazing as % of Façade Area (%)	Glazing as % of Floor Area (%)	Veneer as % of Floor Area (%)			Room Absorption	Incident Sound Angle (deg)	Angle Correction	Source Spectrum	Assumed Veneer (STC)	Building Component	Spectrum Correction	Room Correction	% Total Transmitted Energy (%)	Energy Correction	Building Component		Spectrum Correction	Room Correction	% Total Transmitted Energy (%)	Energy Correction	
Tower 1A L9 to L35 South	Roadway	Daytime	Living/Dining	79	3	45	37	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	54	D	7	-4	5%	51	C	4	-1	95%	0	40	Living / Dining Areas
	Locomotive	Daytime	Living/Dining	68	3	40	31	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	F	54	D	10	-4	5%	48	C	6	-1	95%	0	36	
	Wheel	Daytime	Living/Dining	71	3	40	34	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	B	54	D	2	-4	5%	56	C	1	-1	95%	0	35	
	Roadway	Night-time	Living/Dining	75	3	45	33	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	54	D	7	-4	5%	51	C	4	-1	95%	0	37	
	Locomotive	Night-time	Living/Dining	66	3	40	29	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	F	54	D	10	-4	5%	48	C	6	-1	95%	0	35	
	Wheel	Night-time	Living/Dining	70	3	40	33	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	B	54	D	2	-4	5%	56	C	1	-1	95%	0	34	
	Roadway	Daytime	Sleeping Quarters	79	3	45	37	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	54	D	7	-2	5%	49	C	4	-2	95%	0	40	Sleeping Quarters
	Locomotive	Daytime	Sleeping Quarters	68	3	40	31	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	F	54	D	10	-2	5%	46	C	6	-2	95%	0	36	
	Wheel	Daytime	Sleeping Quarters	71	3	40	34	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	B	54	D	2	-2	5%	54	C	1	-2	95%	0	34	
	Roadway	Night-time	Sleeping Quarters	75	3	40	38	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	54	D	7	-2	5%	49	C	4	-2	95%	0	40	
	Locomotive	Night-time	Sleeping Quarters	66	3	35	34	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	F	54	D	10	-2	5%	46	C	6	-2	95%	0	38	
	Wheel	Night-time	Sleeping Quarters	70	3	35	38	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	B	54	D	2	-2	5%	54	C	1	-2	95%	0	38	
Tower 1A L9 to L35 West																																44	Living / Dining Areas	
	Roadway	Daytime	Living/Dining	74	3	45	32	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	54	D	7	-4	5%	51	C	4	-1	95%	0		35
	Locomotive	Daytime	Living/Dining	64	3	40	27	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	F	54	D	10	-4	5%	48	C	6	-1	95%	0		32
	Wheel	Daytime	Living/Dining	68	3	40	31	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	B	54	D	2	-4	5%	56	C	1	-1	95%	0		31
	Roadway	Night-time	Living/Dining	69	3	45	27	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	54	D	7	-4	5%	51	C	4	-1	95%	0		31
	Locomotive	Night-time	Living/Dining	63	3	40	26	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	F	54	D	10	-4	5%	48	C	6	-1	95%	0		31
	Wheel	Night-time	Living/Dining	67	3	40	30	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	B	54	D	2	-4	5%	56	C	1	-1	95%	0	31	
	Roadway	Daytime	Sleeping Quarters	74	3	45	32	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	54	D	7	-2	5%	49	C	4	-2	95%	0	36	Sleeping Quarters
	Locomotive	Daytime	Sleeping Quarters	64	3	40	27	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	F	54	D	10	-2	5%	46	C	6	-2	95%	0	31	
	Wheel	Daytime	Sleeping Quarters	68	3	40	31	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	B	54	D	2	-2	5%	54	C	1	-2	95%	0	30	
	Roadway	Night-time	Sleeping Quarters	69	3	40	32	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	54	D	7	-2	5%	49	C	4	-2	95%	0	35	
	Locomotive	Night-time	Sleeping Quarters	63	3	35	31	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	F	54	D	10	-2	5%	46	C	6	-2	95%	0	35	
Wheel	Night-time	Sleeping Quarters	67	3	35	35	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	B	54	D	2	-2	5%	54	C	1	-2	95%	0	34		
Tower 1B L9 to L35 North																																39	Living / Dining Areas	
	Roadway	Daytime	Living/Dining	69	3	45	27	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	54	D	7	-4	5%	51	C	4	-1	95%	0		30
	Locomotive	Daytime	Living/Dining	59	3	40	22	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	F	54	D	10	-4	5%	48	C	6	-1	95%	0		28
	Wheel	Daytime	Living/Dining	63	3	40	26	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	B	54	D	2	-4	5%	56	C	1	-1	95%	0		27
	Roadway	Night-time	Living/Dining	64	3	45	22	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	54	D	7	-4	5%	51	C	4	-1	95%	0		25
	Locomotive	Night-time	Living/Dining	58	3	40	21	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	F	54	D	10	-4	5%	48	C	6	-1	95%	0		27
	Wheel	Night-time	Living/Dining	62	3	40	25	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	B	54	D	2	-4	5%	56	C	1	-1	95%	0	26	
	Roadway	Daytime	Sleeping Quarters	69	3	45	27	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	54	D	7	-2	5%	49	C	4	-2	95%	0	29	Sleeping Quarters
	Locomotive	Daytime	Sleeping Quarters	59	3	40	22	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	F	54	D	10	-2	5%	46	C	6	-2	95%	0	26	
	Wheel	Daytime	Sleeping Quarters	63	3	40	26	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	B	54	D	2	-2	5%	54	C	1	-2	95%	0	25	
	Roadway	Night-time	Sleeping Quarters	64	3	40	27	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	54	D	7	-2	5%	49	C	4	-2	95%	0	29	
	Locomotive	Night-time	Sleeping Quarters	58	3	35	26	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	F	54	D	10	-2	5%	46	C	6	-2	95%	0	30	
Wheel	Night-time	Sleeping Quarters	62	3	35	30	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	B	54	D	2	-2	5%	54	C	1	-2	95%	0	29		

Receptor	Source	Time of Day	Location	Sound Levels												Façade and Room Inputs										Source Inputs				Component 1 - Veneer				Component 2 - Glazing					
				Façade Level (dBA)	Free Field Correction (dBA)	Indoor Requirement (dBA)	Required Reduction (dBA)	Exposed Façade Height (m)	Exposed Façade Length (m)	Room Depth (m)	Floor Area (m²)	Façade Area (m²)	Glazing as % of Façade Area (%)	Glazing as % of Floor Area (%)	Veneer as % of Floor Area (%)	Room Absorption	Height of Receptor (m)	Horizontal Distance to Source (m)	Incident Sound Angle (deg)	Angle Correction	Source Spectrum	Assumed Veneer (STC)	Building Component	Spectrum Correction	Room Correction	% Total Transmitted Energy (%)	Energy Correction	Building Component	Spectrum Correction	Room Correction	% Total Transmitted Energy (%)	Energy Correction	Required Glazing (STC)						
Tower 1B L9 to L35 East	Roadway	Daytime	Living/Dining	73	3	45	31	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	54	D	7	-4	5%	51	C	4	-1	95%	0	35	Living / Dining Areas					
	Locomotive	Daytime	Living/Dining	62	3	40	25	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	F	54	D	10	-4	5%	48	C	6	-1	95%	0	31						
	Wheel	Daytime	Living/Dining	66	3	40	29	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	B	54	D	2	-4	5%	56	C	1	-1	95%	0	30						
	Roadway	Night-time	Living/Dining	69	3	45	27	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	54	D	7	-4	5%	51	C	4	-1	95%	0	31						
	Locomotive	Night-time	Living/Dining	60	3	40	23	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	F	54	D	10	-4	5%	48	C	6	-1	95%	0	29						
	Wheel	Night-time	Living/Dining	65	3	40	28	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	B	54	D	2	-4	5%	56	C	1	-1	95%	0	28						
	Roadway	Daytime	Sleeping Quarters	73	3	45	31	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	54	D	7	-2	5%	49	C	4	-2	95%	0	34	Sleeping Quarters					
	Locomotive	Daytime	Sleeping Quarters	62	3	40	25	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	F	54	D	10	-2	5%	46	C	6	-2	95%	0	33						
	Wheel	Daytime	Sleeping Quarters	66	3	40	29	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	B	54	D	2	-2	5%	54	C	1	-2	95%	0	29						
	Roadway	Night-time	Sleeping Quarters	69	3	40	32	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	54	D	7	-2	5%	49	C	4	-2	95%	0	34						
	Locomotive	Night-time	Sleeping Quarters	60	3	35	28	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	F	54	D	10	-2	5%	46	C	6	-2	95%	0	32						
	Wheel	Night-time	Sleeping Quarters	65	3	35	33	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	B	54	D	2	-2	5%	54	C	1	-2	95%	0	32						
Tower 1B L9 to L35 South	Roadway	Daytime	Living/Dining	76	3	45	34	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	54	D	7	-4	5%	51	C	4	-1	95%	0	38	Living / Dining Areas					
	Locomotive	Daytime	Living/Dining	66	3	40	29	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	F	54	D	10	-4	5%	48	C	6	-1	95%	0	35						
	Wheel	Daytime	Living/Dining	69	3	40	32	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	B	54	D	2	-4	5%	56	C	1	-1	95%	0	33						
	Roadway	Night-time	Living/Dining	73	3	45	31	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	54	D	7	-4	5%	51	C	4	-1	95%	0	34						
	Locomotive	Night-time	Living/Dining	64	3	40	27	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	F	54	D	10	-4	5%	48	C	6	-1	95%	0	33						
	Wheel	Night-time	Living/Dining	68	3	40	31	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	B	54	D	2	-4	5%	56	C	1	-1	95%	0	31						
	Roadway	Daytime	Sleeping Quarters	76	3	45	34	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	54	D	7	-2	5%	49	C	4	-2	95%	0	36	Sleeping Quarters					
	Locomotive	Daytime	Sleeping Quarters	66	3	40	29	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	F	54	D	10	-2	5%	46	C	6	-2	95%	0	33						
	Wheel	Daytime	Sleeping Quarters	69	3	40	32	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	B	54	D	2	-2	5%	54	C	1	-2	95%	0	31						
	Roadway	Night-time	Sleeping Quarters	73	3	40	36	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	54	D	7	-2	5%	49	C	4	-2	95%	0	38						
	Locomotive	Night-time	Sleeping Quarters	64	3	35	32	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	F	54	D	10	-2	5%	46	C	6	-2	95%	0	36						
	Wheel	Night-time	Sleeping Quarters	68	3	35	36	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	B	54	D	2	-2	5%	54	C	1	-2	95%	0	35						
Tower 1B L9 to L35 West	Roadway	Daytime	Living/Dining	71	3	45	29	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	54	D	7	-4	5%	51	C	4	-1	95%	0	33	Living / Dining Areas					
	Locomotive	Daytime	Living/Dining	61	3	40	24	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	F	54	D	10	-4	5%	48	C	6	-1	95%	0	30						
	Wheel	Daytime	Living/Dining	65	3	40	28	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	B	54	D	2	-4	5%	56	C	1	-1	95%	0	29						
	Roadway	Night-time	Living/Dining	67	3	45	25	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	54	D	7	-4	5%	51	C	4	-1	95%	0	29						
	Locomotive	Night-time	Living/Dining	60	3	40	23	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	F	54	D	10	-4	5%	48	C	6	-1	95%	0	28						
	Wheel	Night-time	Living/Dining	64	3	40	27	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	60	59.04	2	B	54	D	2	-4	5%	56	C	1	-1	95%	0	28						
	Roadway	Daytime	Sleeping Quarters	71	3	45	29	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	54	D	7	-2	5%	49	C	4	-2	95%	0	31	Sleeping Quarters					
	Locomotive	Daytime	Sleeping Quarters	61	3	40	24	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	F	54	D	10	-2	5%	46	C	6	-2	95%	0	28						
	Wheel	Daytime	Sleeping Quarters	65	3	40	28	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	B	54	D	2	-2	5%	54	C	1	-2	95%	0	27						
	Roadway	Night-time	Sleeping Quarters	67	3	40	30	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	54	D	7	-2	5%	49	C	4	-2	95%	0	32						
	Locomotive	Night-time	Sleeping Quarters	60	3	35	28	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	F	54	D	10	-2	5%	46	C	6	-2	95%	0	32						
	Wheel	Night-time	Sleeping Quarters	64	3	35	32	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	60	59.04	2	B	54	D	2	-2	5%	54	C	1	-2	95%	0	31						









Receptor	Source	Time of Day	Location	Sound Levels				Façade and Room Inputs								Height of Receptor (m)	Horizontal Distance to Source (m)	Source Inputs			Component 1 - Veneer				Component 2 - Glazing				Required Glazing (STC)					
				Façade Level (dBA)	Free Field Correction (dBA)	Indoor Requirement (dBA)	Required Reduction (dBA)	Exposed Façade Height (m)	Exposed Façade Length (m)	Room Depth (m)	Floor Area (m²)	Façade Area (m²)	Glazing as % of Façade Area (%)	Glazing as % of Floor Area (%)	Veneer as % of Floor Area (%)			Room Absorption	Incident Sound Angle (deg)	Angle Correction	Source Spectrum	Assumed Veneer (STC)	Building Component	Spectrum Correction	Room Correction	% Total Transmitted Energy (%)	Energy Correction	Building Component		Spectrum Correction	Room Correction	% Total Transmitted Energy (%)	Energy Correction	
Tower 2AL7 to L35 East	Roadway	Daytime	Living/Dining	71	3	45	29	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	45	D	7	-4	5%	42	C	4	-1	95%	0	33	Living / Dining Areas
	Locomotive	Daytime	Living/Dining	62	3	40	25	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	F	45	D	10	-4	5%	39	C	6	-1	95%	0	31	
	Wheel	Daytime	Living/Dining	66	3	40	29	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	B	45	D	2	-4	5%	47	C	1	-1	95%	0	29	
	Roadway	Night-time	Living/Dining	68	3	45	26	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	45	D	7	-4	5%	42	C	4	-1	95%	0	29	
	Locomotive	Night-time	Living/Dining	60	3	40	23	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	F	45	D	10	-4	5%	39	C	6	-1	95%	0	29	
	Wheel	Night-time	Living/Dining	64	3	40	27	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	B	45	D	2	-4	5%	47	C	1	-1	95%	0	27	
	Roadway	Daytime	Sleeping Quarters	71	3	45	29	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	45	D	7	-2	5%	40	C	4	-2	95%	0	31	36
	Locomotive	Daytime	Sleeping Quarters	62	3	40	25	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	F	45	D	10	-2	5%	37	C	6	-2	95%	0	29	Sleeping Quarters
	Wheel	Daytime	Sleeping Quarters	66	3	40	29	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	B	45	D	2	-2	5%	45	C	1	-2	95%	0	28	
	Roadway	Night-time	Sleeping Quarters	68	3	40	31	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	45	D	7	-2	5%	40	C	4	-2	95%	0	33	
	Locomotive	Night-time	Sleeping Quarters	60	3	35	28	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	F	45	D	10	-2	5%	37	C	6	-2	95%	0	32	
	Wheel	Night-time	Sleeping Quarters	64	3	35	32	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	B	45	D	2	-2	5%	45	C	1	-2	95%	0	31	37
Tower 2AL7 to L35 South	Roadway	Daytime	Living/Dining	70	3	45	28	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	45	D	7	-4	5%	42	C	4	-1	95%	0	32	Living / Dining Areas
	Locomotive	Daytime	Living/Dining	61	3	40	24	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	F	45	D	10	-4	5%	39	C	6	-1	95%	0	30	
	Wheel	Daytime	Living/Dining	65	3	40	28	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	B	45	D	2	-4	5%	47	C	1	-1	95%	0	29	
	Roadway	Night-time	Living/Dining	66	3	45	24	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	45	D	7	-4	5%	42	C	4	-1	95%	0	28	
	Locomotive	Night-time	Living/Dining	60	3	40	23	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	F	45	D	10	-4	5%	39	C	6	-1	95%	0	28	
	Wheel	Night-time	Living/Dining	64	3	40	27	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	B	45	D	2	-4	5%	47	C	1	-1	95%	0	27	
	Roadway	Daytime	Sleeping Quarters	70	3	45	28	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	45	D	7	-2	5%	40	C	4	-2	95%	0	30	Sleeping Quarters
	Locomotive	Daytime	Sleeping Quarters	61	3	40	24	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	F	45	D	10	-2	5%	37	C	6	-2	95%	0	28	
	Wheel	Daytime	Sleeping Quarters	65	3	40	28	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	B	45	D	2	-2	5%	45	C	1	-2	95%	0	28	
	Roadway	Night-time	Sleeping Quarters	66	3	40	29	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	45	D	7	-2	5%	40	C	4	-2	95%	0	31	
	Locomotive	Night-time	Sleeping Quarters	60	3	35	28	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	F	45	D	10	-2	5%	37	C	6	-2	95%	0	32	36
	Wheel	Night-time	Sleeping Quarters	64	3	35	32	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	B	45	D	2	-2	5%	45	C	1	-2	95%	0	31	
Tower 2AL7 to L35 West	Roadway	Daytime	Living/Dining	68	3	45	26	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	45	D	7	-4	5%	42	C	4	-1	95%	0	30	Living / Dining Areas
	Locomotive	Daytime	Living/Dining	58	3	40	21	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	F	45	D	10	-4	5%	39	C	6	-1	95%	0	27	
	Wheel	Daytime	Living/Dining	62	3	40	25	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	B	45	D	2	-4	5%	47	C	1	-1	95%	0	26	
	Roadway	Night-time	Living/Dining	63	3	45	21	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	45	D	7	-4	5%	42	C	4	-1	95%	0	25	
	Locomotive	Night-time	Living/Dining	57	3	40	20	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	F	45	D	10	-4	5%	39	C	6	-1	95%	0	25	
	Wheel	Night-time	Living/Dining	61	3	40	24	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	B	45	D	2	-4	5%	47	C	1	-1	95%	0	25	
	Roadway	Daytime	Sleeping Quarters	68	3	45	26	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	45	D	7	-2	5%	40	C	4	-2	95%	0	28	Sleeping Quarters
	Locomotive	Daytime	Sleeping Quarters	58	3	40	21	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	F	45	D	10	-2	5%	37	C	6	-2	95%	0	29	
	Wheel	Daytime	Sleeping Quarters	62	3	40	25	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	B	45	D	2	-2	5%	45	C	1	-2	95%	0	24	
	Roadway	Night-time	Sleeping Quarters	63	3	40	26	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	45	D	7	-2	5%	40	C	4	-2	95%	0	28	
	Locomotive	Night-time	Sleeping Quarters	57	3	35	25	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	F	45	D	10	-2	5%	37	C	6	-2	95%	0	29	33
	Wheel	Night-time	Sleeping Quarters	61	3	35	29	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	B	45	D	2	-2	5%	45	C	1	-2	95%	0	28	

Receptor	Source	Time of Day	Location	Sound Levels				Façade and Room Inputs								Height of Receptor (m)	Horizontal Distance to Source (m)	Source Inputs			Component 1 - Veneer					Component 2 - Glazing								
				Façade Level (dBA)	Free Field Correction (dBA)	Indoor Requirement (dBA)	Required Reduction (dBA)	Exposed Façade Height (m)	Exposed Façade Length (m)	Room Depth (m)	Floor Area (m²)	Façade Area (m²)	Glazing as % of Façade Area (%)	Glazing as % of Floor Area (%)	Veneer as % of Floor Area (%)			Room Absorption	Incident Sound Angle (deg)	Angle Correction	Source Spectrum	Assumed Veneer (STC)	Building Component	Spectrum Correction	Room Correction	% Total Transmitted Energy (%)	Energy Correction	Building Component	Spectrum Correction	Room Correction	% Total Transmitted Energy (%)	Energy Correction	Required Glazing (STC)	
Tower 2B L7 to L35 North	Roadway	Daytime	Living/Dining	63	3	45	21	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	45	D	7	-4	5%	42	C	4	-1	95%	0	24	Living / Dining Areas
	Locomotive	Daytime	Living/Dining	53	3	40	16	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	F	45	D	10	-4	5%	39	C	6	-1	95%	0	22	
	Wheel	Daytime	Living/Dining	57	3	40	20	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	B	45	D	2	-4	5%	47	C	1	-1	95%	0	21	
																																27		
	Roadway	Night-time	Living/Dining	59	3	45	17	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	45	D	7	-4	5%	42	C	4	-1	95%	0	20	
	Locomotive	Night-time	Living/Dining	51	3	40	14	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	F	45	D	10	-4	5%	39	C	6	-1	95%	0	20	
	Wheel	Night-time	Living/Dining	55	3	40	18	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	B	45	D	2	-4	5%	47	C	1	-1	95%	0	19	
	Roadway	Daytime	Sleeping Quarters	63	3	45	21	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	45	D	7	-2	5%	40	C	4	-2	95%	0	23	Sleeping Quarters
	Locomotive	Daytime	Sleeping Quarters	53	3	40	16	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	F	45	D	10	-2	5%	37	C	6	-2	95%	0	20	
	Wheel	Daytime	Sleeping Quarters	57	3	40	20	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	B	45	D	2	-2	5%	45	C	1	-2	95%	0	19	
	Roadway	Night-time	Sleeping Quarters	59	3	40	22	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	45	D	7	-2	5%	40	C	4	-2	95%	0	24	
	Locomotive	Night-time	Sleeping Quarters	51	3	35	19	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	F	45	D	10	-2	5%	37	C	6	-2	95%	0	23	
Wheel	Night-time	Sleeping Quarters	55	3	35	23	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	B	45	D	2	-2	5%	45	C	1	-2	95%	0	23		
Tower 2B L7 to L35 East	Roadway	Daytime	Living/Dining	75	3	45	33	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	45	D	7	-4	5%	42	C	4	-1	95%	0	36	Living / Dining Areas
	Locomotive	Daytime	Living/Dining	64	3	40	27	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	F	45	D	10	-4	5%	39	C	6	-1	95%	0	33	
	Wheel	Daytime	Living/Dining	68	3	40	31	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	B	45	D	2	-4	5%	47	C	1	-1	95%	0	31	
	Roadway	Night-time	Living/Dining	71	3	45	29	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	45	D	7	-4	5%	42	C	4	-1	95%	0	33	
	Locomotive	Night-time	Living/Dining	62	3	40	25	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	F	45	D	10	-4	5%	39	C	6	-1	95%	0	30	
	Wheel	Night-time	Living/Dining	66	3	40	29	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	B	45	D	2	-4	5%	47	C	1	-1	95%	0	29	
	Roadway	Daytime	Sleeping Quarters	75	3	45	33	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	45	D	7	-2	5%	40	C	4	-2	95%	0	35	Sleeping Quarters
	Locomotive	Daytime	Sleeping Quarters	64	3	40	27	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	F	45	D	10	-2	5%	37	C	6	-2	95%	0	31	
	Wheel	Daytime	Sleeping Quarters	68	3	40	31	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	B	45	D	2	-2	5%	45	C	1	-2	95%	0	30	
	Roadway	Night-time	Sleeping Quarters	71	3	40	34	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	45	D	7	-2	5%	40	C	4	-2	95%	0	36	
	Locomotive	Night-time	Sleeping Quarters	62	3	35	30	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	F	45	D	10	-2	5%	37	C	6	-2	95%	0	34	
	Wheel	Night-time	Sleeping Quarters	66	3	35	34	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	B	45	D	2	-2	5%	45	C	1	-2	95%	0	33	
Tower 2B L7 to L35 South																																39	Living / Dining Areas	
	Roadway	Daytime	Living/Dining	79	3	45	37	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	45	D	7	-4	5%	42	C	4	-1	95%	0		40
	Locomotive	Daytime	Living/Dining	67	3	40	30	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	F	45	D	10	-4	5%	39	C	6	-1	95%	0		35
	Wheel	Daytime	Living/Dining	70	3	40	33	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	B	45	D	2	-4	5%	47	C	1	-1	95%	0	33	
																																42		
	Roadway	Night-time	Living/Dining	75	3	45	33	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	45	D	7	-4	5%	42	C	4	-1	95%	0	37	
	Locomotive	Night-time	Living/Dining	64	3	40	27	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	F	45	D	10	-4	5%	39	C	6	-1	95%	0	33	
	Wheel	Night-time	Living/Dining	68	3	40	31	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	B	45	D	2	-4	5%	47	C	1	-1	95%	0	32	
	Roadway	Daytime	Sleeping Quarters	79	3	45	37	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	45	D	7	-2	5%	40	C	4	-2	95%	0	39	Sleeping Quarters
	Locomotive	Daytime	Sleeping Quarters	67	3	40	30	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	F	45	D	10	-2	5%	37	C	6	-2	95%	0	34	
	Wheel	Daytime	Sleeping Quarters	70	3	40	33	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	B	45	D	2	-2	5%	45	C	1	-2	95%	0	32	
	Roadway	Night-time	Sleeping Quarters	75	3	40	38	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	20	78.69	3	D	45	D	7	-2	5%	40	C	4	-2	95%	0	40	
Locomotive	Night-time	Sleeping Quarters	64	3	35	32	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	F	45	D	10	-2	5%	37	C	6	-2	95%	0	36		
Wheel	Night-time	Sleeping Quarters	68	3	35	36	3.00	3.00	3.00	9.00	9.00	50%	50%	50%	Intermediate	100	120	39.81	1	B	45	D	2	-2	5%	45	C	1	-2	95%	0	35		
Tower 2B L7 to L35 West																																43	Living / Dining Areas	
	Roadway	Daytime	Living/Dining	72	3	45	30	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	20	78.69	3	D	45	D	7	-4	5%	42	C	4	-1	95%	0		34
	Locomotive	Daytime	Living/Dining	61	3	40	24	3.00	3.00	3.00	9.00	9.00	70%	70%	30%	Intermediate	100	120	39.81	1	F	45	D	10	-4	5%	39	C	6	-1	95%	0		30
	Wheel	Daytime	Living																															

## References

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